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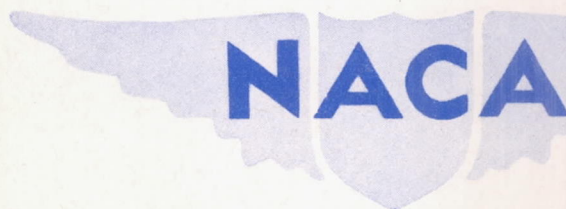
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FLIGHT INVESTIGATION OF THE PERFORMANCE AND COOLING
CHARACTERISTICS OF AN NACA C COWLING ON THE XP-42 AIRPLANE

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MEMORANDUM REPORT

for

Army Air Forces, Materiel Command

FLIGHT INVESTIGATION OF THE PERFORMANCE AND COOLING
CHARACTERISTICS OF AN NACA C COWLING ON THE XP-42 AIRPLANE

By J. Ford Johnston and Stefan A. Cavallo

SUMMARY

Results are presented of high-speed and climb tests of an NACA C cowling on the XP-42 airplane. These tests were made for comparison with tests of NACA type D cowlings on the same airplane.

The top speed corresponding to the engine military power (1000 hp at 14,500 ft) was 336 miles per hour; the addition of Curtiss narrow-chord propeller cuffs increased this speed by 1 mile per hour; and the addition of cuffs and a 24-inch-diameter spinner increased the speed by 3 miles per hour.

Cooling-air-pressure recovery on the front of the engine in climb, at 140 miles per hour indicated airspeed, averaged 58 percent of airplane impact pressure with the spinner and cuffs, 68 percent with cuffs only, and 67 percent without spinner or cuffs. Corresponding pressure recoveries in full-throttle level flight were 69, 74, and 74 percent.

The ground cooling with spinner and cuffs was satisfactory. With cuffs only, spark-plug elbow temperatures exceeded their limit by 29° F after cut-off in the ground run.

Without cuffs or spinner, they exceeded their limit by 65° F, and the oil-in temperature also exceeded its limit.

INTRODUCTION

The NACA has conducted an extensive flight investigation, on the XP-42 airplane, of NACA type D cowlings for radial air-cooled engines. Tests of a long-nose high-inlet-velocity cowling have been reported in reference 1, those of a short-nose high-inlet-velocity cowling in references 2 and 3, and of a short-nose low-inlet-velocity cowling in references 4 and 5. In order to compare these cowlings with the conventional NACA C type now in general use, the flight investigation was extended to include tests of a C cowling, reported herein.

The conditions investigated with the C cowling included:

<u>Test number</u>	<u>Airplane condition</u>
17	C cowling with 24-inch spinner and narrow-chord propeller cuffs - climb
18	C cowling with 24-inch spinner and narrow-chord propeller cuffs - high speed
19	C cowling with cuffs only - high speed
20	C cowling with cuffs only - climb
21	C cowling without spinner or cuffs - climb
22	C cowling without spinner or cuffs - high speed

XP-42 AIRPLANE WITH C COWLING

The XP-42 airplane with its P. & W. 1830 engine was described in reference 2. The C cowl external shape (reference 6) was obtained by adding a lip to the D cowling of references 2, 3, 4, and 5. The internal changes consisted of removing the cowl inner liner and the afterbody of the spinner which together formed the diffuser section typical of the D cowling. A dimensioned drawing of the C cowl installation is given in figure 1. Figures 2 and 3 show the airplane with the spinner and cuffs; figures 4 and 5, with cuffs only; and figures 6 and 7, without spinner or cuffs.

The cuffs and spinner were manufactured by the Propeller Division of the Curtiss-Wright Corporation, and were of the standard design for the 10-foot-diameter Curtiss propeller, drawing number 512 cc 1.5.

The modified cowl flaps used in the tests of references 3, 4, and 5 are shown open in figures 2, 3, and 4, and closed in figures 6 and 7.

TEST APPARATUS

The installation of the test equipment was essentially the same as described in reference 2, with the exception that the three pressure survey rakes which had been installed in the annular diffuser section were moved to a position just forward of the front cylinder-valve push rods at the same

120° intervals around the engine. The left rake may be seen inside the cowling in figure 7.

PROCEDURE

The procedure followed in making the high-speed and climb tests is described in references 2 and 4. For each condition, the high speed was determined from two flights of five runs each. The climb tests for each condition consisted of one climb at 155 miles per hour indicated with the mixture control in automatic rich, and one at 140 miles per hour indicated in the full rich setting, in which the altitude compensator is bypassed.

The ground cooling was checked for each condition by a 10-minute run at 1400 rpm with the cowl flaps open and the propeller in the low-pitch position, followed by a 5-minute idling period. Temperatures were recorded during the runs and for approximately 10 minutes after cut-off.

RESULTS

The data obtained during the high-speed level-flight runs and during the climbs are presented in tables 1(a), 1(b), and 2. Time histories of the climbs are shown in figures 8, 9, and 10.

Analyses of the high-speed performance are given in figures 11 and 12. The observed cooling-air pressure distributions in the high-speed and climb conditions are shown in figures 13 and 14, and typical cylinder-head and barrel temperature distributions, in figures 15 through 18.

Time histories of the ground-cooling tests are presented in figures 19, 20, and 21.

Table 3 gives a comparison of the maximum speeds at military power and the average cooling-air-pressure recoveries with all the cowlings tested on the XP-42 airplane.

DISCUSSION

Maximum Speed

The values of maximum speed and power observed during the full-throttle level runs with each arrangement tested are shown on figure 11. The figure also includes the parameters $\left(\frac{bhp}{\sigma}\right)^{\frac{1}{3}}$, representative of the effective power, and $52.73 \left(\frac{\eta}{C_{DS}}\right)^{\frac{1}{3}}$, representative of the airplane cleanness, as explained in references 1 and 2. The product of these two parameters is the speed of the airplane. The installation having the highest value of the latter parameter will evidently have the highest speed at a given power and altitude.

It was shown in reference 4 that the installation of the modified cowl flaps in the closed position caused an increase of form drag, resulting in a decrease of approximately two-thirds of 1 percent in the parameter $52.73 \left(\frac{\eta}{C_{DS}}\right)^{\frac{1}{3}}$. This increase of drag is attributed to air leakage around the modified flaps and would not be present in a well-designed flap installation. Hence, for comparison with the results of previous tests with the original cowl flaps, it is desirable

to increase by two-thirds of 1 percent the values of speed and $52.73 \left(\frac{\eta}{C_{DS}} \right)^{\frac{1}{3}}$ observed in the present tests. This correction of 2 miles per hour, while not shown on figure 11, has been incorporated in the data plotted on figure 12, which presents a comparison of the speeds obtained with the various cowlings arrangements tested on the XP-42 airplane. Points corresponding to the official performance figures for similar airplanes with conventional air-cooled (P-36A) and liquid-cooled (P-40C) installations are also shown.

Examination of figure 12 shows that if in each case the engine had delivered its rated military power (1000 hp at 14,500 ft; $\frac{bhp}{\sigma} = 1564$), the speeds would have been as listed in table 3. As explained in reference 1, this figure may be used for comparing the speeds of various installations at the same power and altitude by movement of the test points along lines of constant $\frac{\eta}{C_{DS}}$ to a common value of $\frac{bhp}{\sigma}$. Such a comparison at the rated military power of the engine (1000 hp at 14,500 ft; $\frac{bhp}{\sigma} = 1564$) is presented in table 3 for all the cowlings arrangements tested on the XP-42 airplane.

Examination of table 3 shows that the speed with the C cowlings was increased 1 mile per hour by the addition of cuffs and 3 miles per hour by the addition of cuffs and a spinner. It appears that an improvement in the external-flow conditions around the cowl nose was obtained by use of the spinner. The pressure recovery data listed in table 3 indicate

that the cuffs were not loaded in the high-speed condition. It is probable that the cuffs served to streamline the propeller shanks and thus to increase the propulsive efficiency.

It should be noted that the fairing material on the nose of the C cowling (see figs. 3, 5, and 7) was subjected to cracking under flight vibration. Although the fairing was smooth before each high-speed test, some cracks appeared during flight. These cracks would cause a premature transition from a laminar to a turbulent boundary layer and a consequent speed loss estimated at not over 1 mile per hour. No correction has been made for this possible source of drag.

Pressures and Temperatures

The average cooling-air pressures on the front of the engine in full-power level flight with each arrangement are listed in table 3. The pressure recovery at high speed averaged approximately $0.74q_c$ for either case without the spinner, and $0.69q_c$ with cuffs and spinner. Engine cooling-air pressure distributions for the three modifications are shown on figure 13 for the high-speed condition. The values plotted are the average over 10 runs for each location of pressure measurement. The pressures noted on the exhaust side of the barrel of cylinder 3 may be expected to be low because points of measurement lay in the wake of a large ignition cable conduit and next to a hole in the baffling.

The pressures as shown in figure 13 are reasonably uniform, but they are, in general, lower than would be expected from an open-nose cowling. The low inlet velocity in either case without the spinner would preclude any but negligible losses from the cowl entrance to the front of the engine. With the spinner, the inlet velocity ratio is estimated at very nearly 0.25, so that the q at inlet would be $0.06q_c$. An assumption that 90 percent of the inlet q is lost in turbulence due to the lack of a diffuser section behind the spinner leads to the conclusion that the impact pressure at the cowl entrance referred to free-stream static pressure must have been $0.69q_c + 0.05q_c = 0.74q_c$, or the same as that without the spinner.

It appears that about $0.26q_c$ becomes unavailable, as far as the internal pressure recovery is concerned, because of the presence of the propeller ahead of the cowling. Reference 7 shows that the pressure recovery of a model of a similar cowling (with air flow) was $0.97q$ without the propeller, $0.57q$ with a model propeller hub, and $0.62q$ with an operating propeller ahead of the cowling.

As listed in table 3, the pressure recovery on the front of the engine in full-power climb at 140 miles per hour was $0.58q_c$ with spinner and cuffs, $0.68q_c$ with cuffs only, and $0.67q_c$ without cuffs or spinner. Recoveries in climb at 155 miles per hour were the same or $0.01q_c$ higher. It is obvious from these data that the cuffs were ineffective

in climb. The loss due to the spinner was $0.10q_c$. This increased loss is associated with the increase in inlet-velocity ratio in climb as compared with the high-speed condition.

Typical pressure distributions in climb are shown on figure 14. It is noted that the highest pressures occurred on the lower left side of the engine (cylinders 8 to 12) as a result of high angle of attack, slipstream rotation, and the right yaw of the airplane associated with the full-power climb condition. This pressure gradient across the face of the engine is characteristic of the open-nose cowling. When the inlet velocity was increased by use of the spinner, the pressure distribution became more nearly uniform, as may be seen in figure 14. The dumping losses previously noted, however, reduced the general pressure level.

Typical distributions of the cylinder-head and barrel temperatures are shown in figure 15 for the high-speed condition, in figures 16 and 17 for two altitude ranges in the full-rich climb condition, and in figure 18 for the automatic-rich climb. These data have not been corrected to the same conditions, but runs made near the same altitude were selected for each comparison. It appears from these figures that variations in mixture strength and other factors from cylinder to cylinder obscure the effect of variations of cooling-air pressure drop around the engine. It is seen

that the temperature distributions are essentially similar in all cases. Comparison of figures 16 and 17 shows that the distribution becomes more uneven as the mixture strength increases with altitude in the full-rich climb.

Ground Cooling

Time histories of representative temperatures observed during the ground cooling runs are shown in figures 19, 20, and 21 for the cowlings with spinner and cuffs, with cuffs only, and without spinner or cuffs.

In no case with spinner and cuffs did any of the temperatures become critical when corrected to Army standards. However, the oil-in temperature did come within 1° of its limit of 185° F.

In the test with cuffs only, corrected head and barrel temperatures stayed below their Army limits of 500° and 335° F, respectively, but were slightly higher than the spinner-and-cuff condition. The rear spark-plug elbow of cylinder number 7, which was the hottest elbow measured throughout the ground run, ran 29° over its Army limit of 248° F 7 minutes after cut-off.

Without cuffs or spinner, the temperatures of heads and bases were within their limits, but were noticeably higher than with the other two modifications. Spark-plug-elbow temperatures increased throughout the run until at cut-off they were 19° F over their limit and went to 65° F above the

critical temperature 8 minutes after cut-off. Oil-in temperatures also showed a steady increase, passing their critical, when corrected, $7\frac{1}{2}$ minutes after the start of the run and going to 24° F over in 16 minutes, which was the point of cut-off. The magneto operated within its limit throughout the run.

The large change in air temperatures ahead of and behind cylinder number 1, in each case, shows that the air flow reverses direction after the engine is stopped. The fact that in one case (fig. 21) the maximum front spark-plug elbow exceeded even the maximum rear gasket temperature 7 minutes after cut-off is regarded as further evidence of this forward air flow. Comparison of the air temperatures after cut-off in figures 19 and 20 shows that the spinner had no apparent tendency to trap the air in front of the engine.

The cuffs alone improved the ground cooling, and the addition of the spinner gave further improvement. The effect of the spinner was probably to prevent air leakage forward along the propeller shaft.

Langley Memorial Aeronautical Laboratory,
National Advisory Committee for Aeronautics,
Langley Field, Va., November 24, 1942.

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Table (1a) Pressure Data (Sheet 1)

XP-42
AIRPLANE
C COWL
SPINNER &
CLIFFS

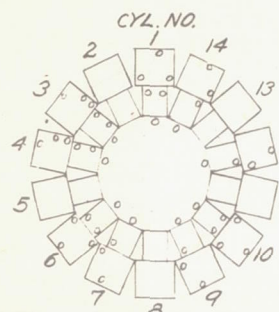
TEST NO. - FLT. NO. RUN NO.		18-5					18-6					IND. AIRSPEED, MPH Q _c	17-4B				17-4A								
TRUE AIRSPEED, MPH Q _c IN. H ₂ O ATM. PRESS. IN. HG. ATM. TEMP. °F Q _t DENSITY RATIO DENSITY ALT., FT. BHP RPM MANIF. PR., IN. HG.		1	2	3	4	5	1	2	3	4	5		1	2	3	4	1	2	3	4					
		334	336	335	333	335	332	332	332	331	333	156	151	153	153	137	137	138	135						
		35.5	34.6	33.3	32.0	31.2	35.3	34.1	33.0	33.3	34.8	12.0	11.3	11.5	11.6	9.3	9.3	9.4	9.0						
		17.53	16.86	16.19	15.56	14.96	17.57	16.88	16.20	16.51	17.22	4900	10000	15100	19000	5200	9900	15100	19000						
		34	34	28	23	21	33	28	24	25	33	63	49	33	18	59	43	28	15						
		6.16	5.92	5.76	5.59	5.40	6.18	6.00	5.81	5.90	6.06	860	880	820	710	870	900	740	620						
		15650	16850	17700	18600	19600	15550	16850	17400	17000	16150	40.0	39.0	36.0	32.9	42.0	42.0	35.0	30.0						
		928	905	872	849	821	919	896	868	886	919	← 2560 →				← 2540 →									
		2680										AUTO RICH CLIMB								FULL RICH CLIMB					
		40.7	39.1	37.8	36.4	35.3	40.5	39.3	37.5	38.4	39.8	WITH SPINNER & CLIFFS													
		HIGH SPEED																							
		PRESSURE RATIO, P ₀₂ /P ₀₁																							
		ENGINE PRESSURE TUBE LOCATIONS																							
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Table 1(a) Pressure Data (Sheet 2)

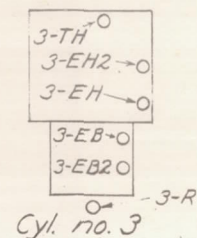
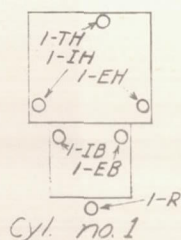
XP-42
AIRPLANE
C COWL
CUFFS ONLY

TEST NO.-FLT. NO.	19-1					19-2					20-1					20-2					
RUN NO.	1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4			
TRUE AIRSPEED, MPH.	332	331	332	330	330	331	331	331	332	334	IND. AIRSPEED, MPH.	155	154	153	152	140	139	139	136		
Q _C IN. H ₂ O	35.0	33.7	32.8	31.4	30.3	34.0	33.0	31.7	30.8	33.9	Q _C	12.0	11.8	11.6	11.5	9.7	9.5	9.5	9.2		
ATM. PRESS. IN. HG.	17.48	16.83	16.16	15.51	14.90	16.89	16.22	15.59	14.94	16.53	AV. PRESS. ALT.	3800	9100	13900	18900	3800	8800	14000	17800		
ATM. TEMP. °F	33	30	27	21	18	26	23	23	20	27	AV. FREE AIR, °F	66	48	34	21	69	48	31	21		
σ, DENSITY RATIO	.616	.596	.576	.560	.541	.603	.583	.560	.540	.589	AV. BHP	870	900	840	750	930	930	780	660		
DENSITY ALT., FT.	15650	16700	17700	18500	19600	16500	17300	18500	19650	17050	AV. MAN. PRESS.										
BHP	928	900	877	849	816	909	877	853	812	905	RPM										
RPM	← 2680 →										← 2580 →					← 2570 →					
MAN. PRESS., IN. HG.	40.5	39.0	37.6	36.3	34.9	39.2	38.0	36.5	35.0	38.6	AUTO RICH CLIMB	WITH CUFFS					FULL RICH CLIMB				
	HIGH SPEED, FULL THROTTLE																				

ENGINE PRESSURE TUBE LOCATIONS



METHOD OF DESIGNATING TUBE LOCATIONS FOR TYPICAL CYLINDERS



PRESSURE RATIO, P_2/P_1									
1-R	2.7	2.6	2.6	2.5	2.6	2.7	2.8	2.6	2.7
3-R	2.7	2.6	2.6	2.5	2.6	2.7	2.8	2.6	2.7
4-R	2.5	2.6	2.6	2.4	2.5	2.7	2.7	2.6	2.6
6-R	2.9	2.8	2.9	2.8	2.8	2.9	2.9	2.8	2.9
7-R	2.9	2.9	3.0	2.8	2.8	3.0	2.9	2.8	2.8
9-R	3.0	2.9	3.0	2.8	2.9	3.1	3.1	3.0	2.9
10-R	3.0	2.9	3.0	2.8	2.9	3.1	3.0	2.9	2.9
12-R	2.7	2.7	2.7	2.6	2.6	2.8	2.8	2.7	2.8
14-R	2.7	2.6	2.6	2.5	2.6	2.7	2.8	2.6	2.7
1-EB	.73	.72	.73	.71	.72	.72	.72	.71	.72
3-EB	.63	.63	.62	.63	.62	.63	.63	.62	.64
4-EB	.73	.73	.73	.73	.73	.72	.72	.73	.74
6-EB	.78	.78	.78	.78	.77	.77	.78	.77	.78
7-EB	.76	.77	.75	.75	.77	.75	.75	.75	.76
9-EB	.79	.79	.80	.78	.80	.78	.80	.78	.79
10-EB	.78	.77	.78	.77	.78	.76	.78	.77	.78
12-EB	.79	.77	.78	.76	.78	.77	.80	.77	.78
14-EB	.79	.80	.79	.78	.78	.79	.80	.78	.79
1-EH	.81	.80	.80	.79	.80	.81	.81	.80	.80
3-EH	.70	.70	.70	.69	.70	.70	.70	.69	.71
4-EH	.74	.75	.74	.75	.74	.74	.74	.73	.76
6-EH	.70	.70	.71	.71	.71	.71	.72	.70	.71
7-EH	.79	.78	.78	.78	.79	.78	.79	.78	.78
9-EH	.76	.75	.76	.76	.76	.76	.77	.75	.75
10-EH	.76	.76	.76	.76	.76	.76	.77	.75	.76
12-EH	.77	.77	.76	.76	.76	.77	.78	.76	.75
14-EH	.79	.79	.78	.77	.79	.79	.80	.79	.78
1-TH	.79	.79	.79	.77	.79	.79	.79	.78	.79
3-TH	.75	.75	.75	.76	.75	.76	.76	.74	.76
4-TH	.75	.75	.75	.74	.75	.76	.75	.74	.73
6-TH	.74	.74	.74	.74	.75	.75	.74	.74	.72
7-TH	.76	.75	.76	.75	.76	.76	.76	.75	.75
9-TH	.80	.79	.79	.79	.80	.79	.80	.78	.79
10-TH	.80	.79	.79	.79	.79	.78	.80	.78	.78
12-TH	.78	.77	.77	.76	.77	.77	.79	.77	.76
14-TH	.73	.73	.73	.73	.73	.73	.74	.73	.72
1-IH	.80	.79	.80	.80	.80	.79	.80	.79	.79
6-IH	.77	.77	.76	.77	.77	.77	.76	.75	.74
10-IH	.79	.79	.80	.78	.80	.79	.81	.78	.79
1-IB	.73	.72	.73	.72	.73	.72	.73	.72	.73
6-IB	.79	.78	.78	.78	.79	.78	.79	.78	.78
10-IB	.77	.77	.77	.78	.76	.76	.79	.77	.75
3-EH2	.63	.63	.64	.63	.63	.63	.62	.63	.64
4-EH2	.71	.72	.70	.71	.71	.72	.70	.71	.69
3-EB2	.58	.58	.58	.58	.59	.58	.59	.58	.58
4-EB2	.60	.61	.60	.61	.60	.59	.59	.60	.61
3-EH2	.34	.34	.35	.34	.34	.34	.34	.35	.34
4-EH2	.31	.31	.32	.31	.31	.31	.31	.32	.31
3-EB2	.58	.58	.58	.58	.59	.58	.59	.58	.58
4-EB2	.60	.61	.60	.61	.60	.59	.59	.60	.61

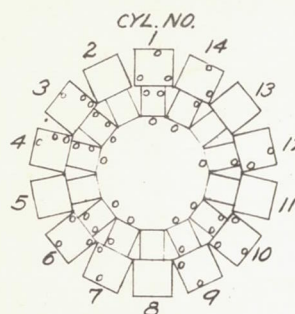
NATIONAL ADVISORY
COMMITTEE FOR AERONAUTICS

Table 1(a) Pressure Data (Sheet 3)

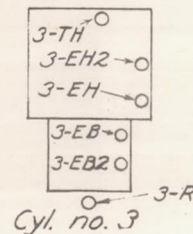
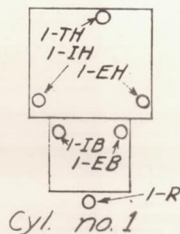
XP-42
AIRPLANE
C COWL
NO CUFFS OR
SPINNER

TEST NO. - FLT. NO. RUN NO.	22-1					22-2					21-1A					21-1B				
TRUE AIRSPEED, MPH.	331	331	331	330	330	329	329	330	330	327	155	153	154	153	139	138	136	135		
Q _c IN. H ₂ O	34.6	33.7	32.3	31.0	30.3	33.9	32.8	31.9	30.8	29.2	11.9	11.6	11.7	11.5	9.5	9.4	9.2	9.0		
ATM. PRESS. IN. HG.	17.23	16.54	15.90	15.27	14.66	17.16	16.47	15.84	15.19	14.60	4200	8900	14200	17800	3900	9700	13800	17700		
ATM. TEMP. °F	28	23	23	19	13	28	26	23	21	19	52	49	37	23	53	51	36	20		
Q _c DENSITY RATIO	616	574	571	553	538	610	588	569	548	529	930	930	840	760	1000	940	740	680		
DENSITY ALT., FT.	15650	16750	17950	18900	19700	15950	17050	18050	19150	20200	39.8	40.0	36.1	31.8	43.0	42.0	36.0	30.8		
BHP	928	900	877	840	816	919	891	863	830	793	2560					2540				
RPM	2680					2680					2560					2540				
MANIF PR., IN. HG.	39.9	38.2	36.8	35.3	34.2	39.7	38.1	36.6	35.3	33.9	AUTO RICH CLIMB NO SPINNER					FULL RICH CLIMB OR CUFFS				

ENGINE PRESSURE
TUBE LOCATIONS



METHOD OF DESIGNATING TUBE LOCATIONS
FOR TYPICAL CYLINDERS



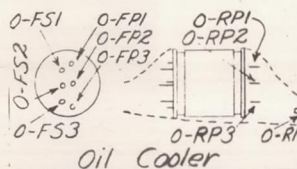
		11000 SPEED										NO SPINNER FOR CUTS									
		PRESSURE RATIO, P/q _c																			
1-R	SHELTERED TUBES BEHIND ENGINE	.22	.22	.23	.22	.22	.25	.26	.24	.23	.25	.38	.38	.35	.36	.45	.45	.40	.46		
3-R		.22	.22	.23	.22	.22	.24	.26	.24	.23	.25	.33	.34	.31	.33	.41	.41	.36	.41		
4-R		.20	.20	.21	.21	.20	.23	.25	.22	.23	.24	.40	.40	.36	.38	.45	.45	.40	.46		
6-R		.25	.26	.26	.26	.26	.29	.30	.28	.27	.29	.23	.21	.20	.23	.28	.29	.23	.31		
7-R		.25	.26	.26	.26	.25	.29	.30	.28	.27	.29	.24	.21	.20	.20	.28	.26	.23	.27		
9-R		.26	.26	.27	.26	.26	.29	.31	.28	.28	.30	.22	.22	.18	.20	.28	.26	.21	.25		
10-R		.26	.26	.27	.26	.26	.29	.30	.28	.27	.30	.25	.24	.22	.24	.32	.30	.23	.27		
12-R		.23	.23	.24	.23	.23	.26	.27	.25	.24	.26	.35	.34	.33	.34	.44	.41	.36	.41		
14-R		.23	.22	.23	.22	.22	.25	.26	.24	.24	.25	.36	.36	.33	.36	.43	.43	.38	.43		
1-EB	EXHAUST SIDE OF BARREL	.72	.72	.72	.72	.72	.73	.73	.72	.73	.73	.52	.53	.56	.56	.49	.52	.54	.53		
3-EB		.61	.62	.62	.61	.62	.62	.63	.61	.63	.63	.43	.43	.46	.45	.40	.39	.45	.41		
4-EB		.71	.73	.74	.72	.73	.73	.74	.72	.74	.73	.67	.68	.71	.70	.66	.71	.70	.66		
6-EB		.76	.76	.78	.77	.77	.77	.79	.77	.78	.79	.74	.75	.78	.77	.73	.74	.79	.75		
7-EB		.75	.75	.76	.76	.76	.76	.78	.76	.74	.78	.68	.71	.72	.70	.70	.72	.72	.71		
9-EB		.78	.79	.79	.79	.78	.79	.81	.80	.79	.81	.75	.77	.81	.78	.75	.80	.82	.79		
10-EB		.77	.76	.77	.77	.77	.77	.79	.78	.78	.78	.77	.75	.78	.76	.81	.79	.84	.79		
12-EB		.78	.79	.79	.78	.78	.79	.80	.79	.79	.80	.67	.65	.70	.69	.70	.73	.77	.74		
14-EB		.80	.79	.80	.78	.78	.80	.80	.80	.80	.80	.66	.66	.69	.69	.58	.68	.67	.67		
1-EH	EXHAUST SIDE OF HEAD	.80	.80	.81	.80	.79	.80	.82	.80	.81	.80	.64	.65	.69	.68	.58	.63	.65	.64		
3-EH		.68	.69	.69	.69	.70	.69	.70	.70	.70	.69	.54	.55	.57	.55	.45	.51	.53	.50		
4-EH		.73	.74	.75	.73	.73	.74	.75	.73	.74	.74	.65	.68	.71	.70	.61	.65	.67	.64		
6-EH		.71	.72	.72	.72	.72	.72	.73	.72	.72	.73	.60	.62	.65	.60	.59	.64	.63	.60		
7-EH		.77	.78	.78	.76	.78	.78	.80	.79	.79	.79	.75	.76	.79	.75	.72	.77	.77	.77		
9-EH		.75	.76	.75	.74	.75	.76	.78	.76	.76	.77	.68	.68	.74	.74	.65	.67	.72	.71		
10-EH		.76	.75	.76	.75	.75	.73	.78	.76	.76	.78	.71	.70	.76	.76	.69	.71	.74	.71		
12-EH		.78	.77	.78	.77	.77	.79	.79	.77	.78	.79	.72	.69	.74	.75	.78	.79	.80	.82		
14-EH		.78	.79	.80	.79	.78	.80	.81	.80	.80	.80	.66	.66	.70	.70	.65	.67	.68	.66		
1-TH	TOP OF HEAD	.78	.80	.80	.79	.79	.81	.82	.81	.81	.81	.66	.66	.70	.69	.63	.64	.64	.61		
3-TH		.74	.75	.76	.74	.75	.75	.76	.74	.75	.76	.66	.70	.72	.69	.63	.67	.64	.63		
4-TH		.75	.76	.76	.75	.75	.75	.78	.74	.76	.77	.68	.70	.76	.74	.67	.70	.72	.68		
6-TH		.75	.75	.76	.75	.75	.76	.77	.76	.76	.77	.69	.70	.76	.73	.68	.72	.72	.68		
7-TH		.76	.76	.76	.75	.76	.76	.78	.76	.76	.77	.70	.73	.76	.74	.69	.71	.74	.71		
9-TH		.79	.79	.79	.79	.80	.80	.80	.79	.81	.81	.76	.76	.80	.80	.73	.76	.80	.78		
10-TH		.82	.78	.80	.79	.78	.80	.80	.78	.80	.82	.76	.77	.80	.80	.73	.75	.78	.78		
12-TH		.78	.78	.79	.78	.78	.80	.80	.78	.80	.80	.75	.72	.76	.76	.73	.76	.80	.80		
14-TH		.73	.74	.75	.74	.74	.75	.76	.76	.76	.75	.57	.56	.61	.61	.55	.55	.63	.62		
1-IB	INTAKE SIDE OF BAR HEAD	.79	.79	.80	.79	.78	.80	.80	.80	.80	.80	.69	.67	.72	.69	.62	.66	.67	.66		
6-IB		.76	.75	.76	.77	.76	.76	.77	.77	.76	.78	.74	.77	.80	.78	.74	.76	.78	.74		
10-IB		.78	.78	.78	.79	.78	.80	.80	.78	.80	.81	.79	.79	.84	.81	.80	.85	.86	.82		
1-IB		.71	.72	.73	.72	.72	.72	.74	.72	.73	.72	.53	.53	.57	.56	.46	.50	.54	.51		
6-IB		.78	.75	.79	.78	.76	.78	.80	.78	.78	.79	.74	.76	.77	.76	.74	.78	.77	.74		
10-IB		.76	.76	.76	.76	.76	.77	.78	.76	.77	.79	.74	.73	.77	.75	.74	.77	.79	.77		
3-EH2		.61	.62	.62	.62	.62	.62	.63	.62	.64	.62	.40	.43	.44	.44	.34	.42	.38	.35		
4-EH2		.71	.72	.72	.72	-	.71	.73	.72	.71	.72	.63	.64	.66	.63	.57	.61	.61	.60		
3-EB2		.56	.56	.57	.56	.56	.57	.58	.57	.58	.59	.29	.33	.35	.33	.22	.27	.29	.31		
4-EB2		.57	.59	.61	.59	.60	.60	.60	.61	.61	.60	.43	.52	.56	.56	.46	.50	.48	.43		

Table 1(b) Pressure Data (Sheet 1)

XP-42
AIRPLANE
C COWL
SPINNER &
CUFFS

TEST NO.- FLT NO.		18-3					18-2					17-4B					17-4A				
RUN NO.		1	2	3	4	5	1	2	3	4	5	1	2	3	4	1	2	3	4		
TRUE AIRSPEED		334	336	335	333	335	332	332	332	331	333	156	151	153	153	137	137	138	135		
Qc. INCHES H ₂ O		355	346	333	320	312	353	341	330	333	348	12.0	11.3	11.5	11.6	9.3	9.3	9.4	9.0		
ATM. PRESS IN. HG		17.53	16.86	16.19	15.56	14.96	17.57	16.88	16.20	16.51	17.22	4900	10000	15100	19000	5200	9900	15100	19000		
ATM TEMP °F		34	34	28	23	21	33	28	24	25	33	63	44	33	18	59	43	28	15		
DENSITY RATIO		.616	.592	.576	.559	.540	.618	.600	.581	.590	.606	860	880	820	710	870	900	740	620		
DENSITY ALT., FT.		15450	16350	17700	19600	19600	15550	16450	17400	17000	16150	40.0	39.0	36.0	30.9	42.0	40.0	35.0	30.0		
BIP		928	905	872	849	821	919	896	868	886	919	2560					2540				
RPM		2680										AUTO RICH CLIMB					FULL RICH CLIMB				
MANIF. PR. IN HG		40.7	39.1	37.8	36.4	35.3	40.5	39.3	37.5	38.4	39.8	SPINNER AND CUFFS									
		HIGH SPEED																			
		PRESSURE RATIO P/qc																			
3 TSI ENGINE O.D.	A-TPI	65	66	64	63	63	66	65	65	65	65	52	52	54	54	52	55	52	56		
	A-TS	65	64	64	63	62	65	64	64	65	64	51	52	52	53	52	53	52	53		
		64	63	62	62	62	65	63	63	61	63	50	52	51	58	56	59	53	52		
		69	70	69	69	67	72	71	70	71	70	65	65	67	65	71	69	66	69		
		71	78	77	76	75	76	77	76	77	78	67	65	70	65	65	69	68	69		
	A-RPI	67	61	64	64	62	65	64	64	64	64	44	51	52	53	48	49	48	49		
		67	64	64	62	62	65	64	64	64	63	67	72	68	68	63	65	71	70		
		63	63	61	61	60	63	62	62	62	62	62	69	63	67	59	65	66	66		
		72	71	69	69	68	70	71	69	71	70	47	51	54	55	48	50	51	52		
	A-RS	70	68	68	68	67	70	70	69	70	69	60	60	63	63	62	60	63	64		
66		64	64	63	63	66	65	64	65	65	53	53	53	68	50	50	49	52			
66		65	66	64	63	66	66	64	65	65	42	50	52	53	45	49	50	49			
63		64	62	62	61	62	63	62	63	62	69	71	72	72	70	69	69	69			
A-LP	65	64	63	63	62	65	64	64	65	64	63	70	68	73	64	65	67	68			
	70	70	69	69	68	70	70	69	69	70	51	55	57	58	53	52	51	52			
	72	71	71	71	68	72	72	71	72	71	51	55	52	60	52	50	49	50			
	65	64	64	63	62	65	65	64	64	61	52	55	54	54	52	52	51	54			
BOTTOM BARRELS d of	A-LP	65	64	64	63	62	65	64	64	64	64	63	70	68	73	64	65	67	68		
	A-LS	69	70	69	69	67	72	71	70	71	70	51	55	57	58	53	52	51	52		
		65	64	64	63	62	65	65	64	64	64	63	70	68	73	64	65	67	68		
		68	67	66	66	65	67	67	67	67	67	52	55	54	54	52	52	51	54		
		64	64	64	62	62	64	64	64	64	64	63	70	68	73	64	65	67	68		
	O-FP	62	62	62	62	61	62	62	62	62	62	63	63	63	63	62	60	63	64		
		65	65	63	63	62	66	64	65	65	65	48	50	52	53	45	49	50	49		
		85	86	84	85	84	85	86	85	85	84	99	96	94	89	107	99	102	100		
		90	92	91	91	91	91	92	92	92	91	103	102	100	96	116	106	104	101		
	O-FS	98	96	95	94	95	96	97	96	97	95	102	104	101	96	109	110	104	104		
80		79	80	79	78	81	81	81	81	80	73	82	82	79	88	87	84	86			
80		80	80	80	79	81	83	81	82	81	79	83	84	79	87	87	85	86			
84		84	83	83	82	84	84	81	84	83	82	82	82	79	92	89	82	86			
O-RP	60	60	58	57	57	60	60	58	59	59	37	38	36	36	44	39	43	36			
	52	54	53	52	52	53	55	54	55	53	22	25	27	26	30	30	28	27			
	71	70	69	67	67	71	70	69	71	70	63	61	62	56	63	65	64	60			
	51	51	51	50	49	52	52	52	51	51	22	23	24	22	30	27	25	23			
C-PI	89	88	90	87	88	90	90	88	89	89	93	87	89	88	103	86	88	88			
	91	91	92	89	88	91	90	92	92	92	100	92	91	91	103	91	96	94			
	94	92	92	92	93	94	94	94	95	92	100	103	101	94	114	101	99	98			
	97	94	94	95	94	95	96	96	96	94	102	108	107	100	118	112	103	107			
	97	94	94	94	94	96	96	96	96	94	112	113	106	104	118	112	111	109			
C-SI	73	73	72	72	71	72	72	73	73	73	71	58	56	57	64	41	43	48			
	72	70	71	70	69	71	70	71	71	71	65	56	53	55	59	33	40	43			
	69	69	69	68	69	70	70	70	70	71	57	62	62	58	62	32	39	42			
	69	68	69	68	69	69	70	70	70	70	55	61	62	56	61	32	39	42			
	69	69	68	68	68	69	69	69	70	69											
C-TH	IMPACT	72	74	75	73	72	74	73	73	74	74	72	54	58	57	67	37	48	51		
	IN CORR																				

A diagram illustrating the layout of various probes (A-TP5, A-TP4, A-TP1, A-TS3, A-TS1, A-LP, A-RP5, A-RS3) relative to the engine's outer diameter (O.D.). The diagram shows concentric circles representing the engine's profile, with labels for 'TOP OF BARRELS' and 'BOTTOM OF BARRELS'. Arrows indicate the direction of the probes towards the engine.



Carburetor Scoop
"C-55"

- C-P5 o
C-P4 o o C-S4
C-P3 o o C-S3
C-P2 o o C-S2
C-P1 o
-
- C-S1

TABLE II(b) PRESSURE DATA (SHEET 2)

TEST NO. - FLT. NO.		19-1					19-2					20-1					20-2				
RUN NO.		1	2	3	4	5	1	2	3	4	5	1	2	3	4	5	1	2	3	4	5
TRUE AIRSPEED		332	331	332	330	330	331	331	331	332	334	155	154	153	152	152	140	139	139	136	136
Q. INCHES H ₂ O		350	337	328	314	303	340	330	317	308	339	12.0	11.8	11.6	11.5	11.5	9.7	9.5	9.5	9.5	9.2
ATM. PRESS. IN. HG		17.48	16.83	16.16	15.51	14.90	16.89	16.22	15.59	14.94	16.53	3800	4100	13400	18700	18700	3800	3800	44000	17800	
ATM. TEMP. °F		53	50	47	44	41	36	33	33	30	27	66	48	40	34	31	69	48	31	21	21
DENSITY RATIO		0.716	0.706	0.696	0.686	0.676	0.703	0.693	0.683	0.673	0.663	0.970	0.900	0.840	0.750	0.750	0.930	0.930	0.780	0.660	0.660
DENSITY ALT., FT		15650	16700	17700	18700	19700	16500	17300	18100	18900	19700	970	900	840	750	750	930	930	780	660	660
R.P.M.		405	390	376	363	349	392	380	365	350	386	← 2580 CUFFS ONLY					← 2570 FULL RICH CLIMB ONLY				
MANIF. PR. IN. HG		40.5	39.0	37.6	36.3	34.9	39.2	38.0	36.5	35.0	38.6										
A-TS1		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS2		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS3		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS4		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS5		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS6		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS7		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS8		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS9		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS10		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS11		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS12		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS13		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS14		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS15		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS16		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS17		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS18		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS19		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS20		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS21		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS22		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS23		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS24		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS25		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS26		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS27		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS28		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS29		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS30		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS31		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS32		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS33		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS34		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS35		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS36		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS37		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS38		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS39		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS40		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS41		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS42		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS43		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS44		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS45		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS46		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS47		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS48		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS49		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS50		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS51		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS52		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS53		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS54		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS55		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS56		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS57		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS58		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS59		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS60		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS61		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS62		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14	14	14	15
A-TS63		15	15	15	15	15	14	14	14	14	15	15	15	15	15	15	14	14			

TABLE 1(b) PRESSURE DATA (SHEET 3)

TEST NO. - FLT. NO.		22-1					22-2					21-1A		21-1D	
RUN NO		1	2	3	4	5	1	2	3	4	5	1	2	3	4
TRUE AIRSPEED		331	331	331	330	330	329	329	330	330	327	155	153	154	153
Q.C. INCHES H ₂ O		346	337	323	310	303	339	328	319	308	29.2	9.5	11.6	11.7	9.4
ATM. PRESS. IN. HG		1723	1654	1590	1527	1416	1716	1647	1584	1519	14.60	3900	8900	14200	17800
ATM. TEMP. °F		38	33	23	19	13	38	26	23	21	19	52	49	37	53
C.D. DENSITY RATIO		1.16	1.04	0.94	0.87	0.80	1.16	1.04	0.94	0.87	0.80	930	930	840	760
DENSITY ALT., FT.		15650	16750	17950	19900	23700	15950	17050	18050	19150	20200	398	400	361	319
BHP		428	400	377	340	316	419	391	363	330	293	430	420	360	308
MANIF. PR. IN. HG		399	382	368	353	342	391	381	366	353	339	2560			
		PRESSURE HIGH					RATIO P/q					NO SPINNER OR CUFFS			
		PRESSURE					RATIO P/q					AUTO RICH CLIMB			
		PRESSURE					RATIO P/q					FULL RICH CLIMB			
		PRESSURE					RATIO P/q								
		PRESSURE					RATIO P/q								
		PRESSURE					RATIO P/q								
		PRESSURE					RATIO P/q								
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TABLE 2		TEMPERATURE DATA (SHEET 1)																			
TEST NO - FLIGHT NO. RUN NO.		18-5					18-6					17-4B					17-4A				
TRUE AIRSPEED, M.P.H.		1	2	3	4	5	1	2	3	4	5	1	2	3	4	5	1	2	3	4	5
Qc IN H ₂ O		334	336	335	333	335	332	332	332	331	333	154	152	154	154	154	140	138	137	135	135
ATM. PRESS. IN. HG.		35.5	34.6	33.3	32.0	31.2	35.3	34.1	33.0	33.3	34.8	11.7	11.4	11.7	11.7	11.7	9.6	9.4	9.3	9.0	9.0
ATM. TEMP. °F		17.53	16.86	16.19	15.56	14.96	17.57	16.88	16.20	16.51	17.22	5000	10700	15400	18800	18800	6600	10200	16000	19100	19100
DENSITY RATIO		34	34	28	23	21	33	28	24	25	33	63	47	32	19	19	55	43	26	15	15
DENSITY ALT., FT.		616	592	576	559	540	618	600	581	590	606	860	900	810	710	710	928	890	718	639	639
B.H.P.		15650	16850	17700	18600	19600	15550	16450	17400	17000	16150	400	391	356	310	310	43.2	41.5	33.9	30.0	30.0
R.P.M.		928	905	872	849	821	919	896	868	886	919	2560					2540				
MAN. PRESS IN. HG		40.7 39.1 37.8 36.4 35.3					40.5 39.3 37.5 36.4 39.8					AUTO RICH CLIMB					FULL RICH CLIMB				
CYL. NO. PT. OF MEASUREMENT		TEMP °F					TEMP °F					TEMP °F					TEMP °F				
1 - REAR 3P. PL. GASKET		397	389	391	399	422	392	389	398	398	398	328	393	412	424	424	390	386	346	335	335
2		382	382	387	394	418	387	387	396	396	396	324	384	397	402	402	375	370	337	321	321
3		397	394	399	403	430	396	394	403	401	401	335	395	408	419	419	390	384	350	337	337
4		399	394	399	403	432	401	396	403	398	396	321	399	399	412	412					
5																					
6		394	392	399	403	425	396	396	408	408	410	335	386	399	408	408	377	370	353	353	353
7		448	452	455	461	487	455	454	465	465	465	375	443	466	470	470	426	424	417	404	404
8		416	419	423	426	451	422	419	431	429	433	355	408	430	437	437	406	404	393	381	381
9												330	381								
10		429	430	437	439	462	438	435	447	445	447	359	417	442	446	446	406	404	399	386	386
11		442	442	448	451	480	446	445	456	456	456	361	424	450	457	457	410	408	399	390	390
12		414	416	421	426	448	419	419	431	431	433	350	406	428	433	433	395	393	381	368	368
13																					
14																					
1 - REAR 1/2 BARREL FLANGE		314	313	314	317	328	320	313	317	317	317	355	410	426	430	430	399	393	355	341	341
2							316	313	315	313	317	267	299	315	319	319	297	290	281	279	279
3		307	306	309	312	321	311	304	308	308	308	263	294	306	312	312	292	292	279	272	272
4		309	309	312	314	326	314	318	315	313	315	269	299	310	312	312	297	294	283	279	279
5		295	296	298	300	313	302	296	301	299	304	254	281	294	290	290	279	279	272	267	267
6		312	310	314	316	328	314	310	315	315	317	265	297	310	315	315	290	294	288	283	283
7		307	306	309	312	321	311	306	308	310	313	260	290	294	306	306	285	288	285	279	279
8		302	303	307	309	321	304	301	306	304	308	258	292	294	310	310	285	290	288	281	281
9		323	324	325	327	340	325	325	326	326	329	272	306	319	324	324	297	299	297	292	292
10		330	332	332	337	347	334	329	336	336	338	279	312	330	332	332	306	310	310	301	301
11		305	306	304	309	319	309	304	308	306	309	265	292	306	310	310	285	288	285	279	279
12																					
13		307	308	309	314	324	311	318	313	313	315	269	297	312	315	315	292	292	288	277	277
14		317	320	321	321	335	320	317	322	325	326	274	306	315	321	321	297	299	288	279	279
10 MIX. AT INTAKE PORT		237	230	232	229	227	232	230	230	233	233	219	219	222	220	220	226	213	201	194	194
" " BLOWER RIM		164	168	168	177	169	174	168	168	171	174	161	174	171	168	168	179	171	161	152	152
FUEL - SUC. SIDE PUMP		92	96	96	99	99	90	93	96	96	99	79	79	76	76	76	79	79	79	79	79
" - PR. " "		95	99	99	102	102	93	99	100	102	102	79	79	76	79	79	82	79	79	76	76
" - CARB. FLOAT CHAMBER		90	93	93	93	96	91	93	93	96	96	82	79	72	72	72	82	79	72	72	72
" - FRT. 3P. ELBOW		66	64	63	63	57	66	63	60	63	66	82	72	59	52	52	82	72	55	45	45
" - REAR " " "		84	84	84	81	81	87	84	81	84	87	99	92	82	79	79	103	92	79	72	72
RECORDED FREE AIR		50	50	47	42	39	51	45	42	44	48	70	54	38	26	26	60	50	33	24	24
AIR - CARB. SCOOP		51	51	48	42	39	54	48	40	45	51	72	55	38	28	28	65	55	35	24	24
" - FRT. CYL. 14		49	48	45	42	39	51	45	42	45	51	72	55	38	28	28	65	55	35	24	24
" - FRT. CYL. 1		57	60	57	57	57	60	60	57	57	60	76	59	45	38	38	69	59	42	35	35
" - REAR " " "		148	151	154	157	163	154	151	163	157	157	165	174	174	178	178	175	171	161	155	155
" - OIL COOLER EXIT		84	84	84	81	81	89	84	84	84	87	89	89	79	69	69	92	86	72	65	65
OIL - IN LINE		148	146	148	145	148	154	147	146	146	148	148	139	135	135	135	139	139	132	129	129
OIL - OUT		219	217	219	219	225	217	217	217	217	219	144	203	210	210	210	205	203	200	197	197
ACCESSORY COMPT.		119	119	119	119	122	122	119	119	119	124	102	99	89	86	86	106	99	86	79	79
LEFT MAGNETO		107	108	108	107	105	112	109	108	108	110	96	96	92	92	92	96	96	92	86	86
PILOT'S COCKPIT		102	102	105	102	102	99	100	102	99	102	79	79	69	65	65	82	79	69	65	65
RECORDING INSTR. COMPT.		87	90	93	90	90	87	90	89	75	90	82	82	76	69	69	86	83	72	69	69

TABLE 2

TEMPERATURE DATA (SHEET 2)

TEST NO.-FLIGHT NO. RUN NO.		TEMPERATURE DATA (SHEET 2)																							
		19-1					19-2							20-1				20-2							
TRUE AIRSPEED, MPH		332	331	332	330	330	331	331	331	332	334	IND. AIRSPEED		154	153	153	151	138		135	136	136			
Qc IN. H ₂ O		35.0	33.7	32.8	31.4	30.3	34.0	33.0	31.7	30.8	33.9	Qc IN. H ₂ O		11.7	11.5	11.5	11.2	9.4		9.0	9.1	9.1			
ATM. PRESS. IN. HG		17.48	16.83	16.16	15.51	14.90	16.89	16.22	15.59	14.94	16.53	AVE. PRESS. ALT.		4600	10800	14700	18800	4000		9700	14900	18600			
ATM. TEMP. °F		33	30	27	21	18	26	23	23	20	27	AVE. FREE AIR °F		62	42	31	19	67		44	28	19			
DENSITY RATIO		.616	.596	.576	.560	.541	.603	.583	.560	.540	.589	AVE. B.H.P.		850	905	807	720	939		900	758	650			
DENSITY ALT., FT		15650	16700	17700	18500	19600	16500	17300	18500	19650	17050	AVE. MANIF. PRESS.													
B.H.P.		928	900	877	849	816	909	877	853	812	905	R. P. M.													
R.P.M.		2680												2580				2570							
MAN. PRESS IN. HG		40.5					39.0	37.6	36.3	34.9	39.2	38.0	36.5	35.0	38.6	AUTO RICH CLIMB				FULL RICH CLIMB					
		HIGH SPEED					HIGH SPEED							CUFFS ONLY											
CYL. NO PT. OF MEASUREMENT		TEMP. °F																							
1	- REAR SP. PL. GASKET	377	375	378	382	388	389	383	397	393	379		387	403	401	401	376	381	352	331					
2		375	375	379	382	388	383	389	399	395	381		387	403	398	394	381	381	352	329					
3		384	379	384	388	393	392	395	409	406	388		392	410	407	403	390	386	358	336					
4																									
5																									
6		379	377	382	384	386	381	390	399	395	386		385	396	394	390	374	376	361	339					
7		434	432	436	439	443	440	444	458	452	438		430	449	455	452	424	431	420	401					
8		395	395	400	400	402	399	406	418	411	404		401	413	419	413	390	399	388	372					
9																									
10		420	420	424	427	429	424	430	442	436	429		412	427	436	432	401	410	404	384					
11		427	427	432	436	439	438	440	454	444	436		419	434	443	441	404	410	404	386					
12		402	404	407	412	416	410	417	429	420	414		396	407	412	407	390	390	376	358					
13																									
14																									
1	- REAR & BARREL FLANGE	307	302	304	304	311	305	313	318	318	300		298	311	311	311	283	297	290	278					
2		309	300	307	309		302	304	311	309	295		288	305	305	305	283	299	285	280					
3		302	295	298	298	302	302	304	311	309	295		298	311	311	309	283	292	285	278					
4		304	300	304	304	307	304	307	313	313	295		298	311	311	309	285	297	288	278					
5		293	286	288	291	293	293	295	300	300	283		279	290	290	290	267	280	274	267					
6		307	304	304	304	309	304	309	315	315	297		290	307	309	309	280	294	292	285					
7		302	295	298	298	300	302	302	306	309	290		287	300	300	300	274	288	285	278					
8		298	293	295	295	298	293	295	302	302	286		279	295	298	298	271	283	285	278					
9		316	313	316	316	320	318	318	327	325	311		300	317	322	322	288	304	302	297					
10		325	325	325	327	327	325	329	336	334	318		309	324	327	329	292	315	313	304					
11		298	295	295	295	300	302	302	306	306	293		288	300	302	302	276	290	288	278					
12																									
13		304	300	302	302	304	304	304	313	311	297		288	300	302	302	278	290	285	276					
14		313	309	311	313	316	316	316	322	322	309		300	313	316	316	288	299	290	283					
10	MIX. AT INTAKE PORT	221	219	219	219	219	219	222	225	223	223		229	220	215	211	225	211	204	194					
	" " BLOWER RIM	169	163	160	160	160	167	164	164	167	162		177	179	174	165	166	181	169	155					
	FUEL - SUC. SIDE PUMP	89	92	92	92	92	88	91	96	93	93		82	79	79	76	84	84	84	81					
	" - PR. " "	92	94	94	94	94	93	93	96	96	99		82	82	79	76	87	84	84	81					
	" - CARB. FLOAT CHAMBER	89	89	89	89	89	88	88	91	93	91		82	79	76	73	87	81	78	75					
11	- FRT. SP. PL. ELBOW	68	65	62	59	59	64	62	64	62	64		85	68	62	50	84	78		46					
12	- REAR " " "	77	74	73	71	68	73	70	73	70	76		102	88	79	68	107	90	75	64					
	RECORDED FREE AIR	48	46	42	39	36	44	41	41	38	44		66	48	38	22	70	50	36	25					
	AIR - CARB. SCOOP	51	48	45	42	39	47	41	44	41	47		68	50	36	24	73	55	37	19					
	" - FRT. CYL. 14	51	45	42	42	36	44	41	41	38	44		68	50	36	24	73	55	37	19					
	" - FRT. CYL. 1	54	51	51	45	42	50	47	47	44	50		76	56	47	33	78	60	46	37					
	" - REAR " " "	143	141	146	149	154	139	142	148	148	139		177	179	179	177	183	186	144	133					
	" - OIL COOLER EXIT	83	80	80	77	74	82	79	79	79	79		93	82	76	65	93	87	75	60					
	OIL - IN LINE	146	141	138	138	138	142	139	142	148	139		144	138	135	132	147	141	135	133					
	OIL - OUT	219	214	214	214	214	217	212	217	217	209		204	215	215	209	197	205	202	197					
	ACCESSORY COMPT.	116	115	115	112	112	114	114	116	114	114		107	96	90	82	107	98	87	78					
	LEFT MAGNETO	106	106	103	103	103	105	102	105	102	99		96	93	90	85	98	95	90	84					
	PILOTS COCKPIT	94	94	94	92	92	93	93	93	93	93		85	79	76	70	93	84	78	69					
	RECORDING INSTR. COMPT.	74	73	71	68	68	82	85	85	88	85		90	82	76	70	95	87	78	69					

TABLE 2

TEMPERATURE DATA (SHEET 3)

TEST NO.- FLIGHT NO. RUN NO.	22-1					22-2					IND. AIRSPEED Q _c	21-1A				21-1B			
	1	2	3	4	5	1	2	3	4	5		1	2	3	4	1	2	3	4
TRUE AIRSPEED M. P. H.	331	331	331	330	330	329	329	330	330	327	155	153	152	152	140	137	135	135	
Q _c IN. H ₂ O	346	337	323	310	303	339	328	319	308	292	11.8	114	113	113	96	92	90	89	
ATM. PRESS., IN. HG.	17.23	16.54	15.90	15.27	14.66	17.16	16.47	15.84	15.19	14.60	46.00	9400	14200	17600	5200	8700	14300	17700	
ATM. TEMP., °F	28	23	23	19	13	28	26	23	21	19	52	47	37	24	55	53	35	19	
ρ, DENSITY RATIO	.616	.594	.571	.553	.538	.610	.588	.569	.548	.529	941	930	845	762	1019	933	771	680	
DENSITY ALT., FT.	15650	16750	17950	18900	19700	15950	17050	18050	19150	20200	39.8	39.9	36.1	31.9	42.9	43.1	35.5	30.8	
B. H. P.	928	900	877	840	816	919	891	863	830	793	2560				2540				
R. P. M.	2680					2680					AUTO RICH CLIMB				FULL RICH CLIMB				
MANIF. PRESS., IN. HG.	399	382	368	353	342	397	381	366	353	339	NO SPINNER				OR CUFFS				
CYL. NO.- PT. OF MEASUREMENT	TEMP., °F					HIGH SPEED						HIGH SPEED				HIGH SPEED			
1 - REAR 3P. PL. GASKET	369	367	372	374	379	377	368	373	377	377		383	406	406	406	361	390	352	338
2	369	365	372	374	379	373	366	370	373	375		381	401	397	394	359	385	350	332
3	374	366	374	379	383	377	370	375	379	382		390	403	399	397	366	390	356	341
4												390	399	390	390	361	383	350	332
5																			
6	374	369	374	376	379	373	373	375	377	377		383	399	394	392	363	381	361	345
7	430	428	430	434	434	430	428	430	435	435		439	453	457	455	412	434	419	401
8	394	392	394	394	397	393	390	393	397	397		403	419	421	417	383	403	390	376
9																372	392	403	397
10	423	419	426	426	428	419	419	423	426	426		417	437	448	443	401	419	412	394
11	423	421	428	428	432	422	422	426	428	430		421	441	450	452	401	419	408	397
12	401	397	403	403	407	397	397	401	404	404		401	419	424	421	383	397	385	370
13																			
14																			
1 - REAR 2 BARREL FLANGE	313	327	306	306	306	312	303	303	305	305		296	309	312	325	294	303	294	282
2																			
3	302	293	293	297	299	301	294	294	296	298		289	303	305	305	289	298	289	280
4	304	299	299	302	304	303	301	301	303	303		294	309	309	307	296	305	291	282
5	291	286	286	288	288	291	287	287	290	290		280	294	294	294	280	287	278	271
6	304	302	302	302	304	303	301	303	303	305		291	307	309	309	294	303	298	289
7	302	295	297	297	297	301	296	296	298	298		287	298	303	300	282	291	284	278
8	293	288	291	291	288	294	290	291	291	291		284	298	303	303	284	294	289	282
9	320	313	315	315	318	319	314	314	314	316		303	318	325	323	303	309	309	303
10	327	325	325	327	327	327	325	325	325	327		307	330	336	332	314	327	323	314
11	299	293	295	295	297	294	291	294	294	296		287	300	305	305	289	294	291	284
12																			
13	302	297	297	297	299	301	298	298	301	301		289	303	309	305	291	296	291	282
14	313	309	311	311	313	312	310	310	312	312		300	318	323	321	303	309	298	289
10-MIX. AT INTAKE PORT	219	215	215	215	215	218	218	216	216	216		223	221	221	213	221	213	204	195
" " BLOWER RIM	168	157	157	157	154	166	164	155	158	161		166	174	172	169	169	174	166	158
FUEL- SUCTION SIDE PUMP	81	84	84	84	84	85	88	91	91	93		77	77	77	77	77	77	77	74
" PRESS. " "	86	86	86	89	89	91	93	91	93	96		80	80	77	77	77	77	77	74
" CARB. FLOAT CHAMBER	81	81	81	81	81	85	88	82	88	88		80	74	77	74	74	77	74	72
11 - FRT. 3P. PL. ELBOW	64	64	57	57	52	64	64					74	77	68	60	71	74	66	53
11 - REAR " " "	75	69	69	66	64	73	76	68	68	68		91	91	83	74	88	94	83	71
RECORDED FREE AIR	46	40	40	36	31	47	46	41	38	38		57	52	42	30	60	58	42	26
AIR CARB. SCOOP	46	43	40	38	34	47	46	41	38	38		60	54	43	28	60	57	40	28
" FRT. CYL. NO. 14	46	43	40	38	34	47	46	41	38	38		60	57	43	28	60	60	43	28
" FRT. CYL. NO. 1	57	55	55	55	55	56	56	50	47	41		66	66	54	46	68	66	54	43
" REAR " " "	118	115	115	118	120	119	119	119	122	127		144	152	152	150	150	155	147	149
" OIL COOLER EXIT	84	78	78	72	72	82	82	72	76	76		88	88	83	74	97	97	83	57
OIL - IN LINE	145	140	140	137	137	150	144	142	142	142		147	144	144	142	142	147	144	139
" OUT	220	214	212	212	212	221	216	208	213	216		204	210	215	215	204	199	210	204
ACCESSORY COMP'T.	115	109	109	109	106	113	113	111	111	111		100	100	94	86	97	100	91	83
LEFT MAGNETO	101	101	95	93	95	105	105	96	99	99		91	91	91	88	94	97	97	91
PILOT'S COCKPIT.	89	89	86	86	84	85	91	88	85	85		80	77	71	68	74	77	72	51
RECORDING INSTR. COMP'T.	81	81	81	81	78	71	71	68	68	64		80	77	74	68	77	80	80	54

Table 3: Speed and Pressure Recovery Data from Flight Investigations of XP-42 Airplane.

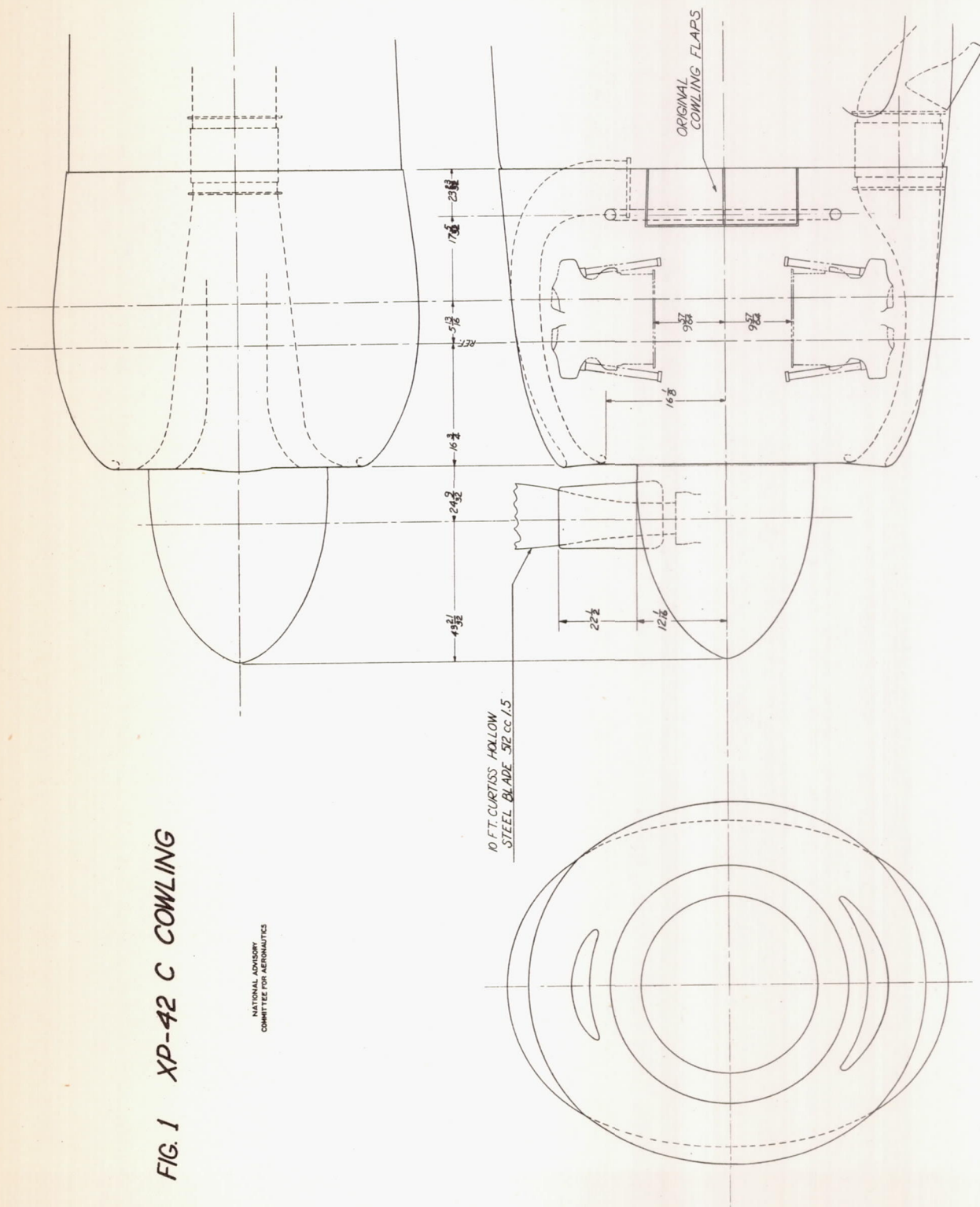
	Long Nose	S.N.-H.I.V.		S.N.-L.I.V.					C-Cowl		
	with cuffs	Cuffs	No Cuffs	Fan and #1 Cuffs	Fan Only	#1 Cuffs	#2 Cuffs	No Cuffs	Spinner Cuffs	Cuffs Only	No Cuffs or Spinner
①	344	339	340	337	339	339	342	343	339	337	336
②	.83	.80	.74	.87	.84	.80	.77	.76	.69	.74	.74
③	.86	.70	.62	1.02	.98	.86	.84	.74	.58	.68	.67
④	.83	.70	.62	.95	.95	.81	.82	.75	.58	.69	.68

- ① Maximum Speed at 1000hp. at 14500 ft.-mph true airspeed
- ② Pressure recovery on front of engine at high speed, P/q_c
- ③ Pressure recovery in 140-mph, (indicated airspeed) climb
- ④ Pressure recovery in 155-mph climb (indicated airspeed)

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FIG. 1 XP-42 C COWLING

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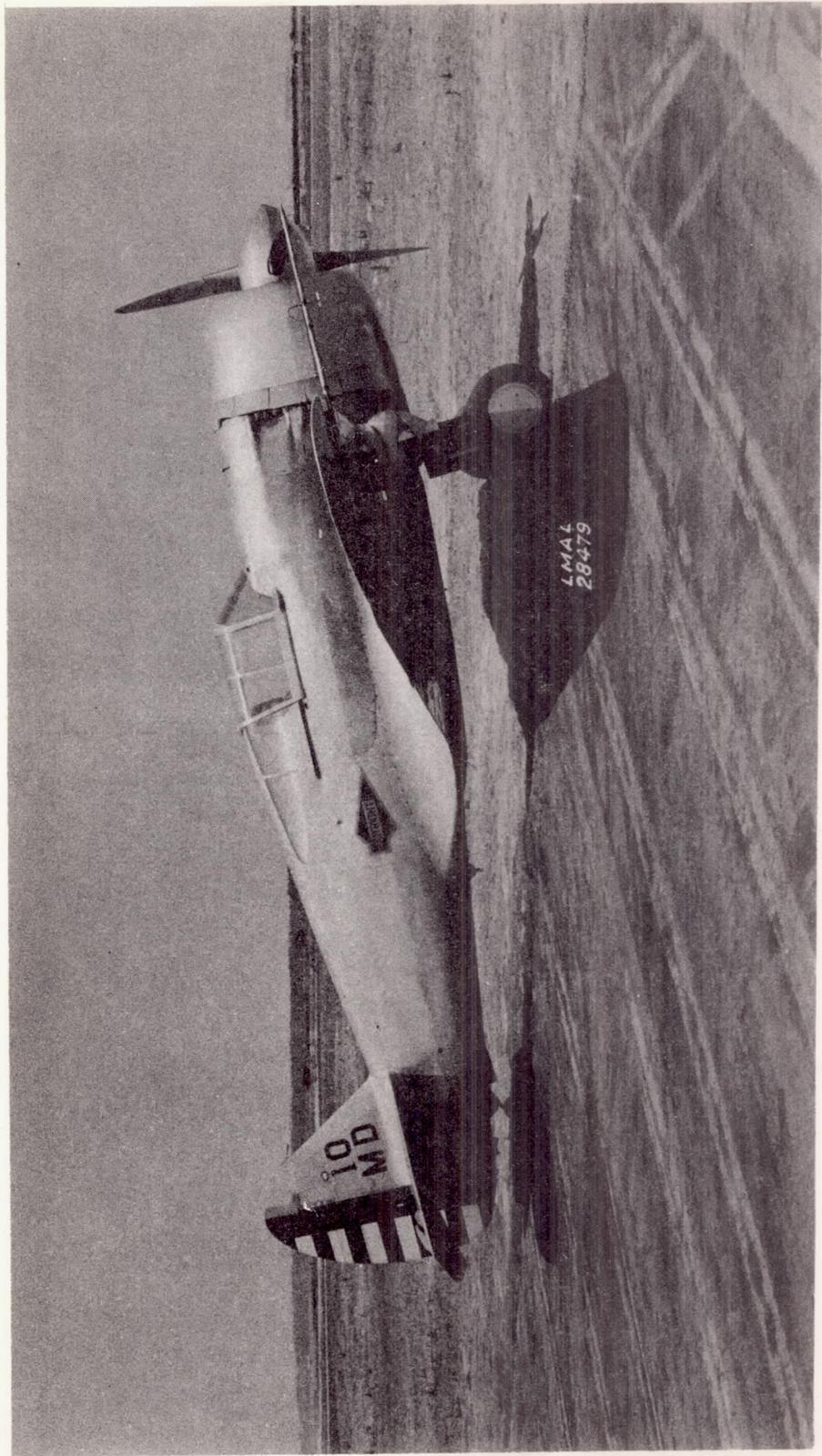


Figure 2.- Side view of airplane with C cowl, spinner, and cuffs.

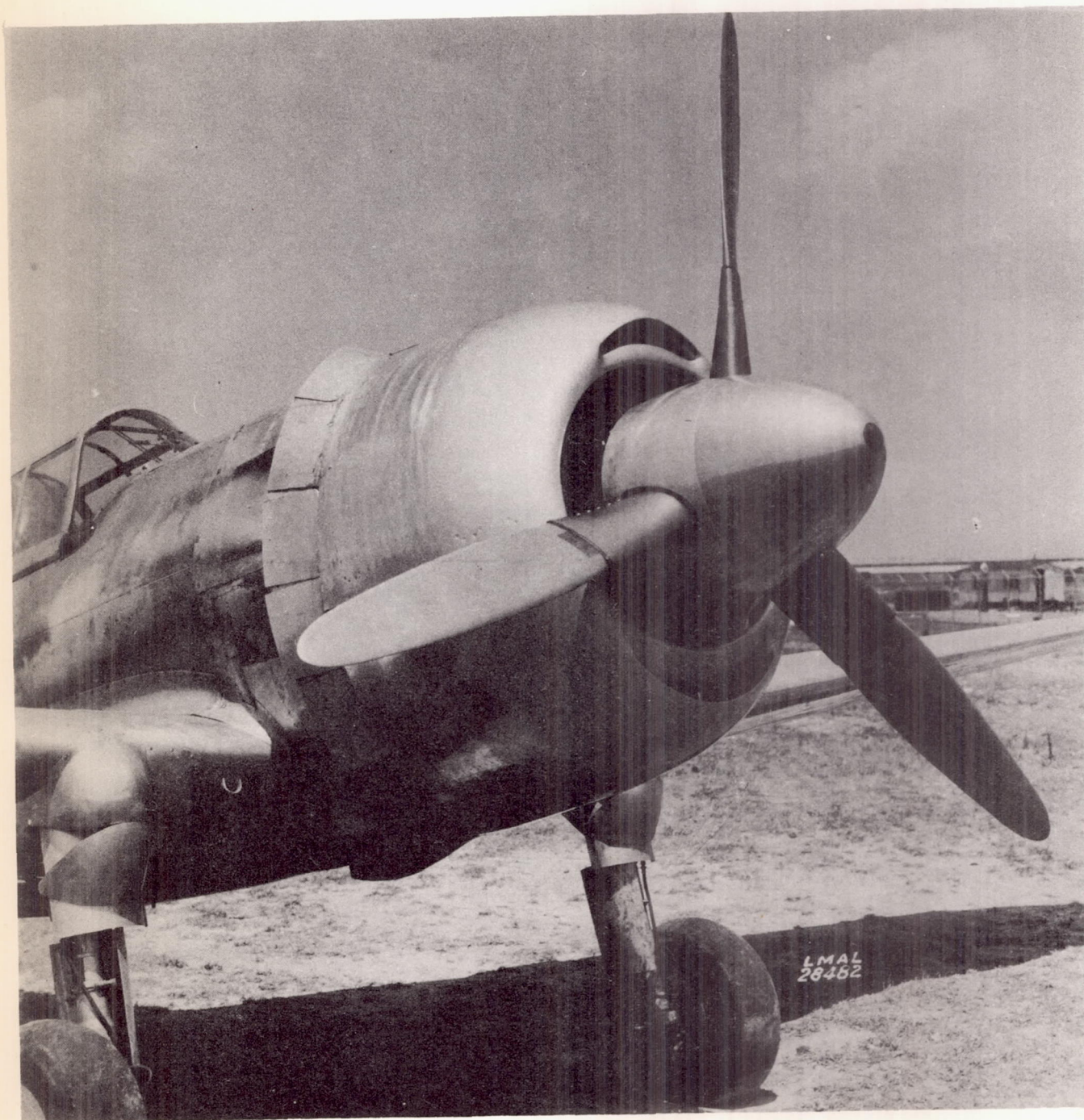


Figure 3.- Close-up of cowling with spinner and cuffs.

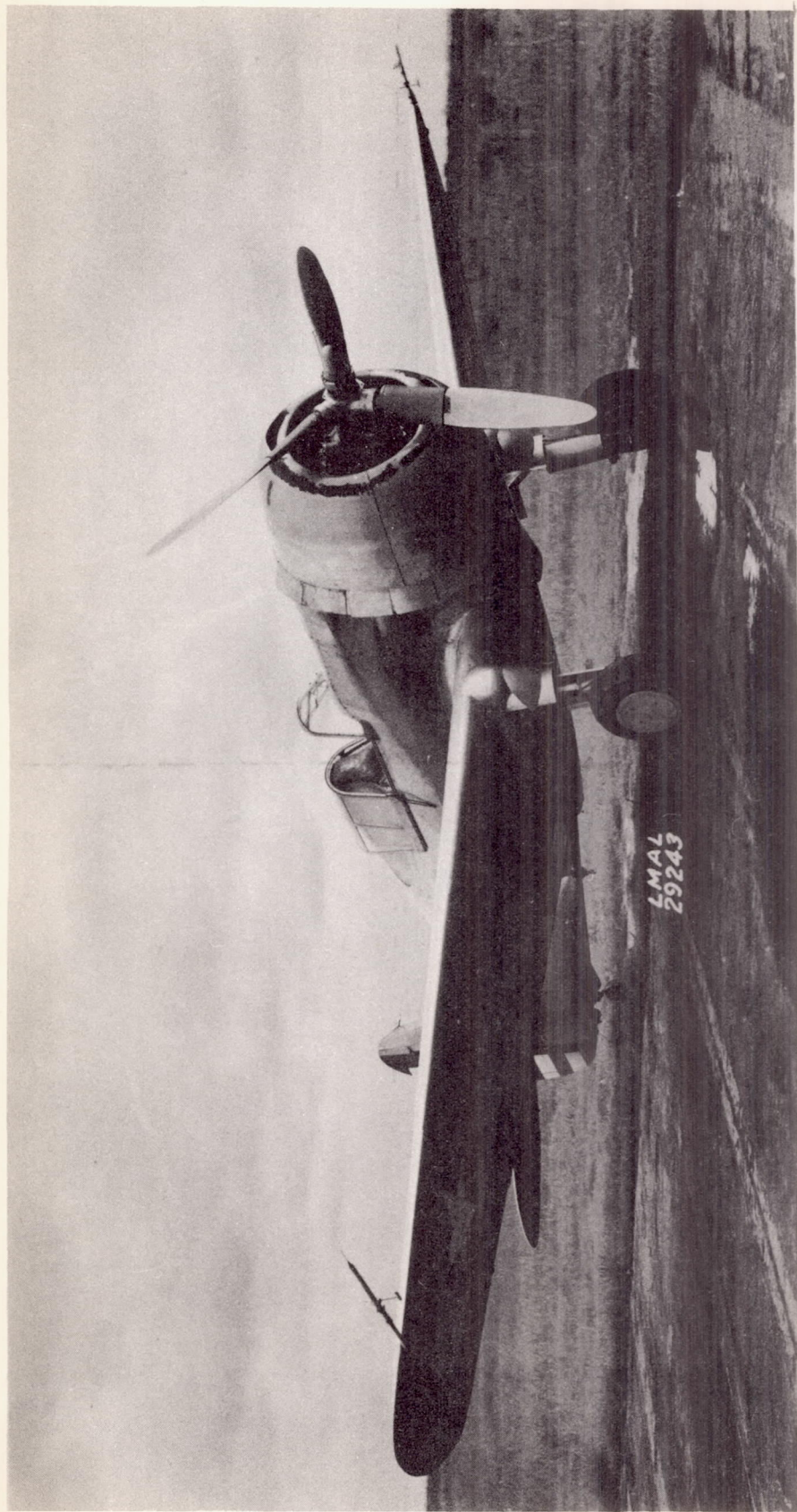


Figure 4.- Three-quarter front view of airplane with C cowl, cuffs only.

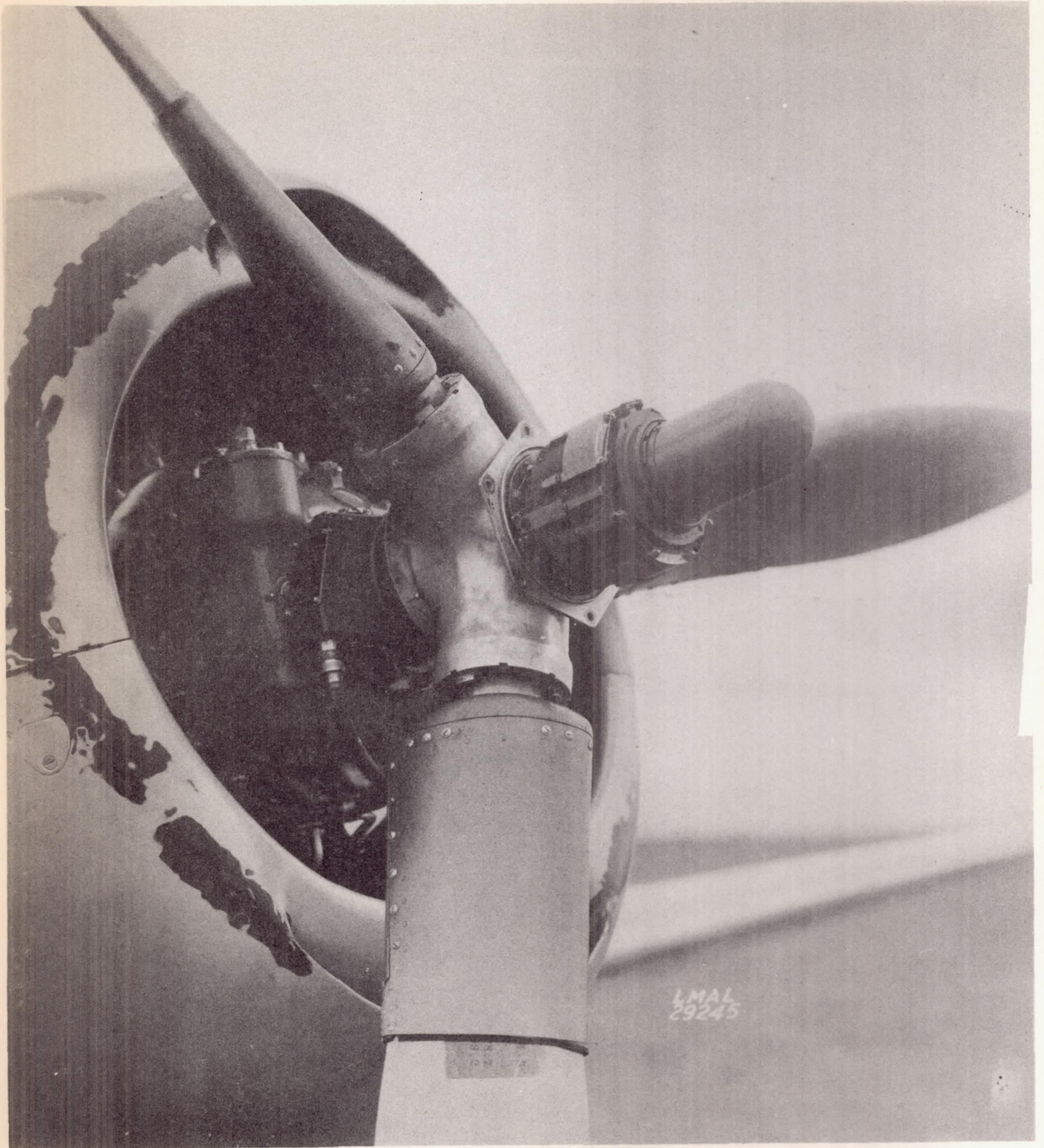


Figure 5.- Close-up of cowling with cuffs only.

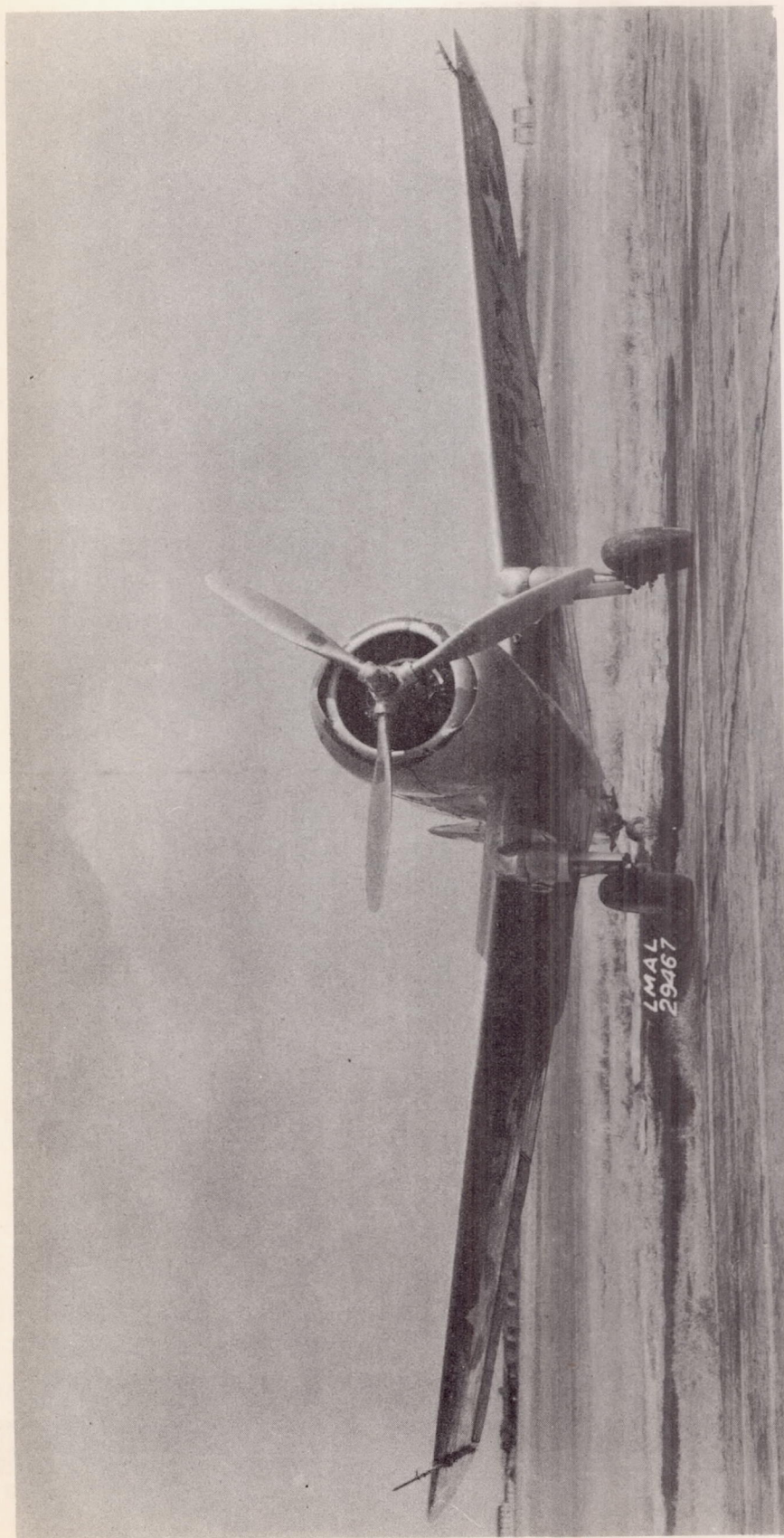


Figure 6.- Front view of cowling without spinner or cuffs.



Figure 7.- Close-up of cowling without spinner or cuffs.

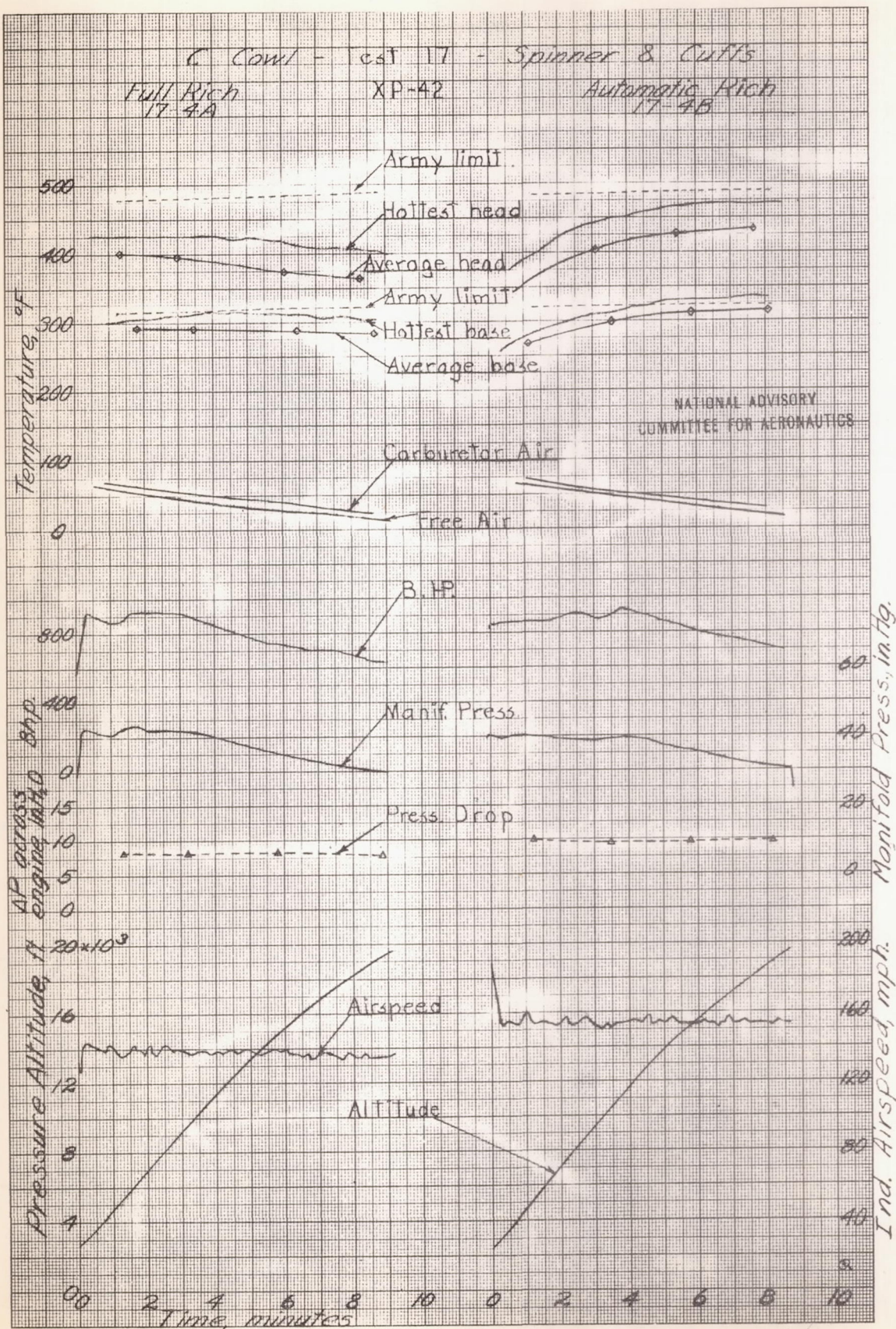
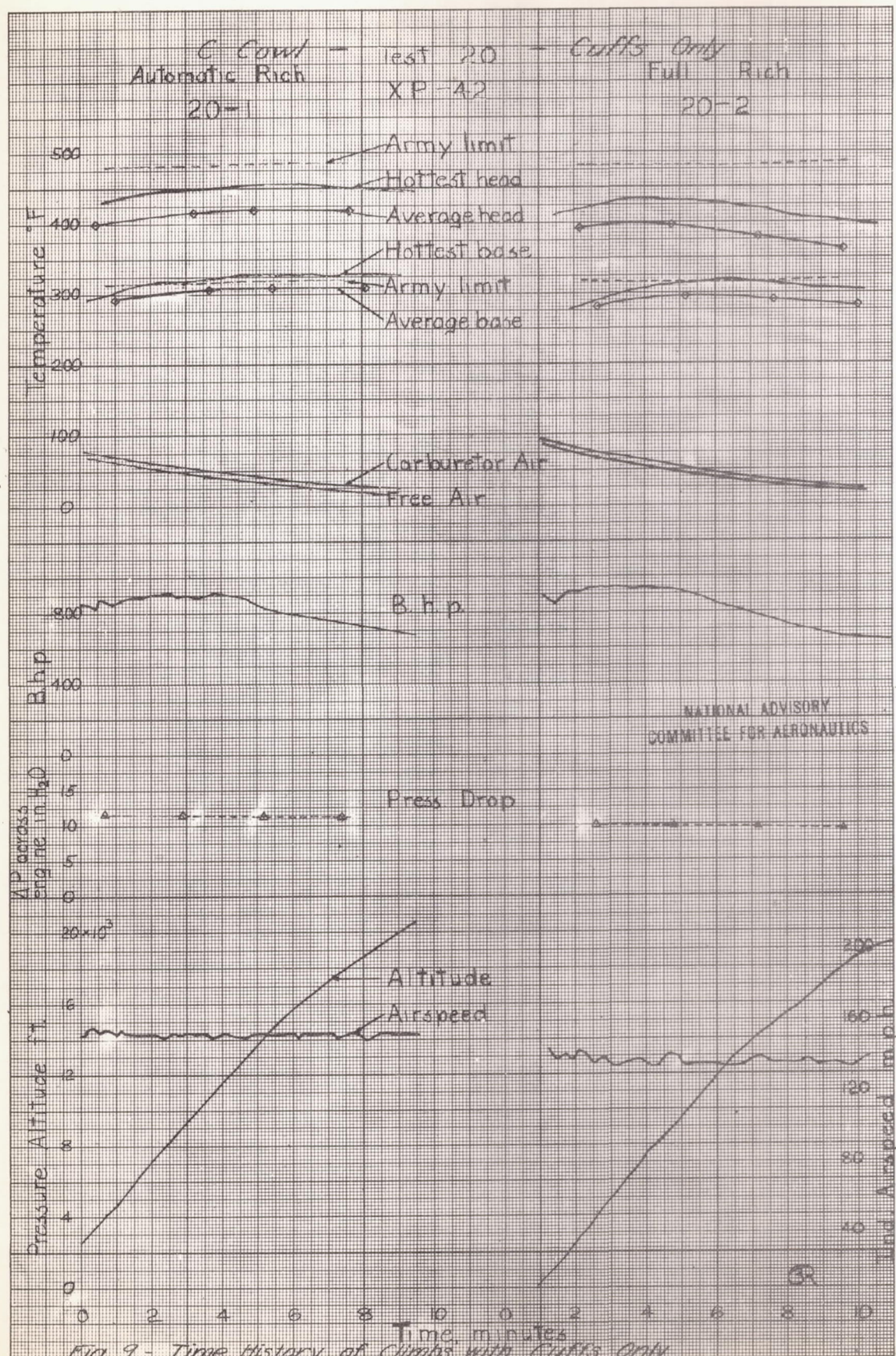
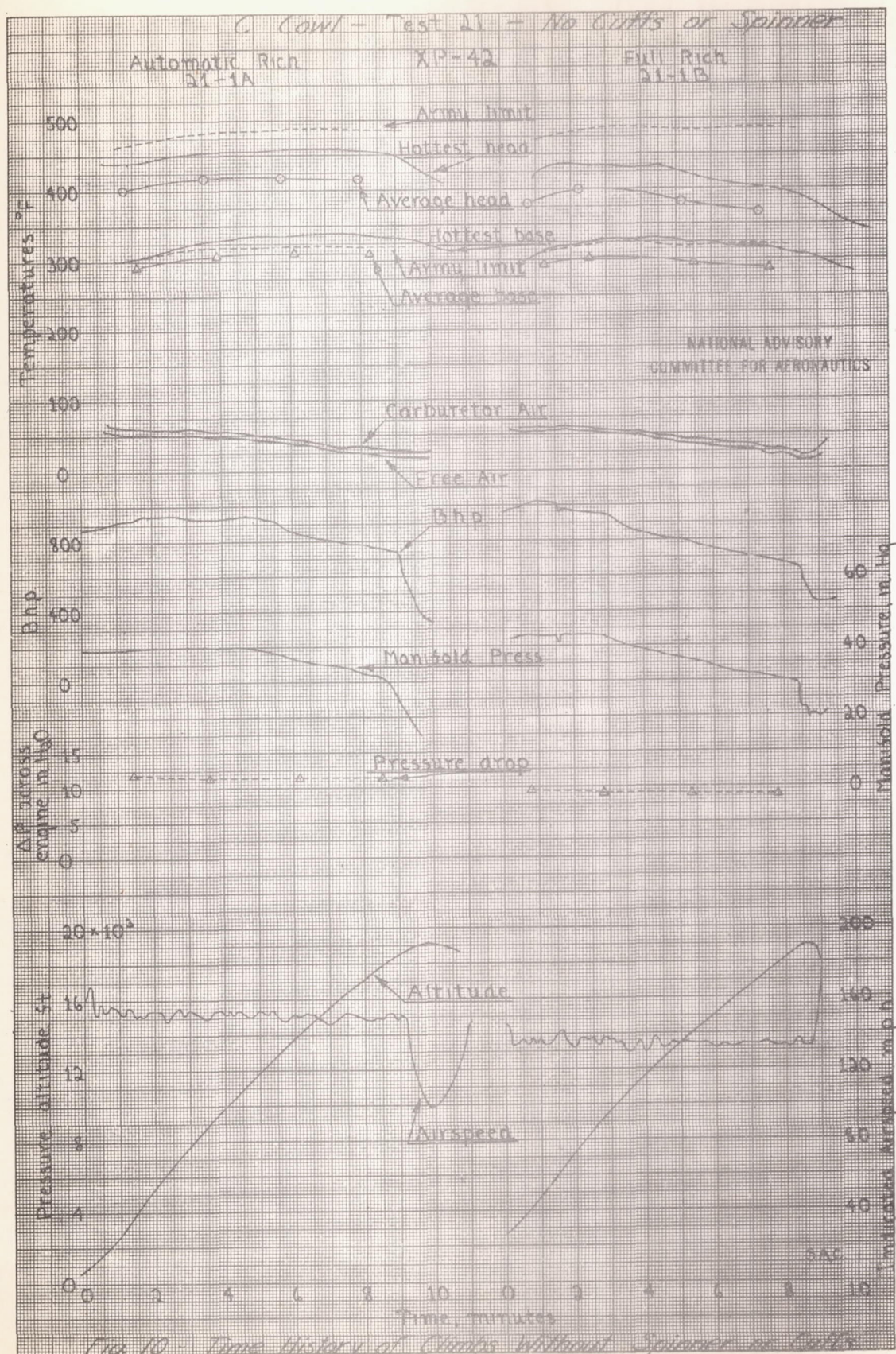
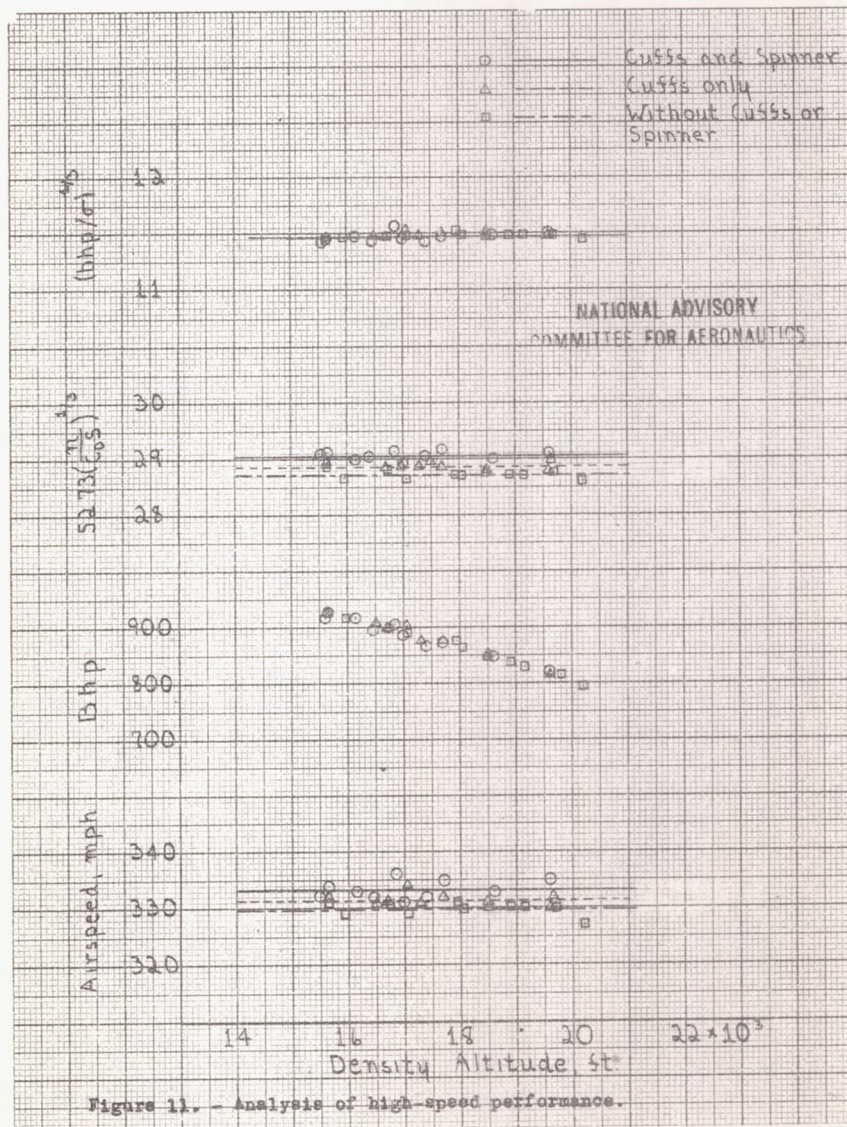


Fig. 8 Time History of Climbs with Spinner & Cuffs







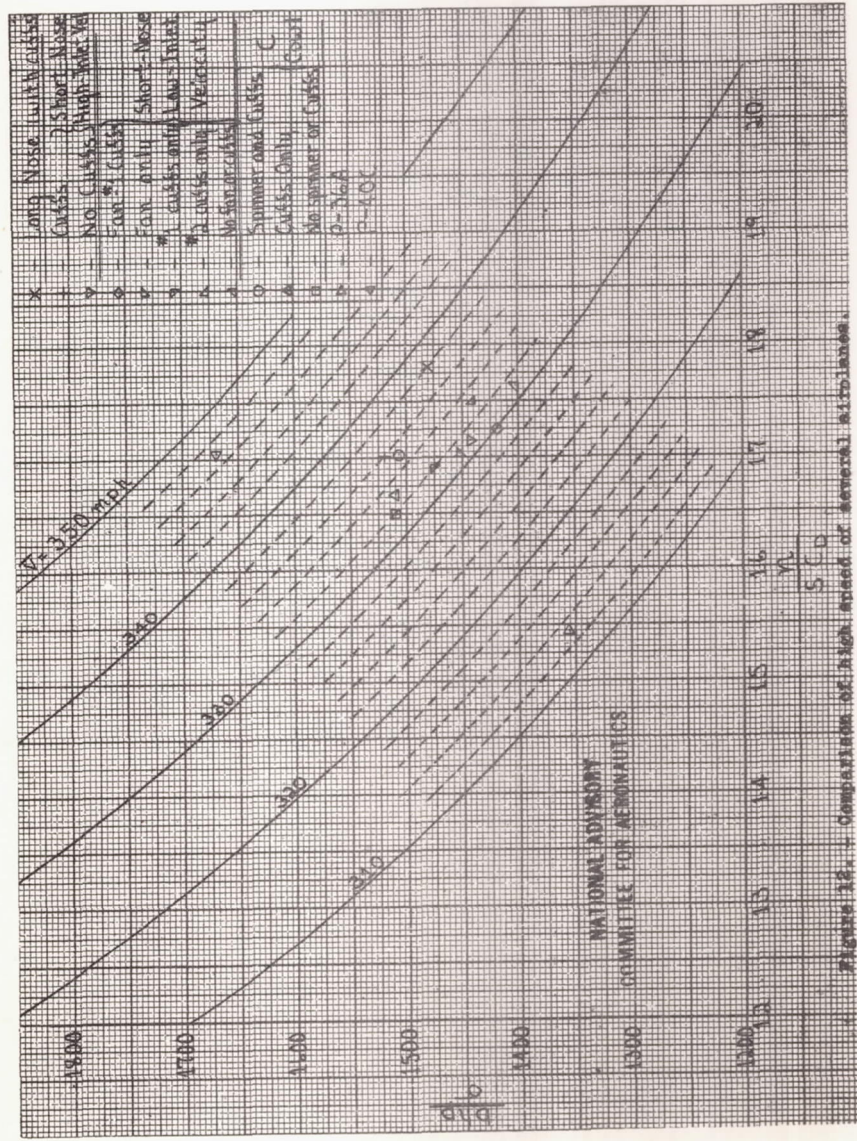


Figure 12. - Comparison of high speed of several airplane.

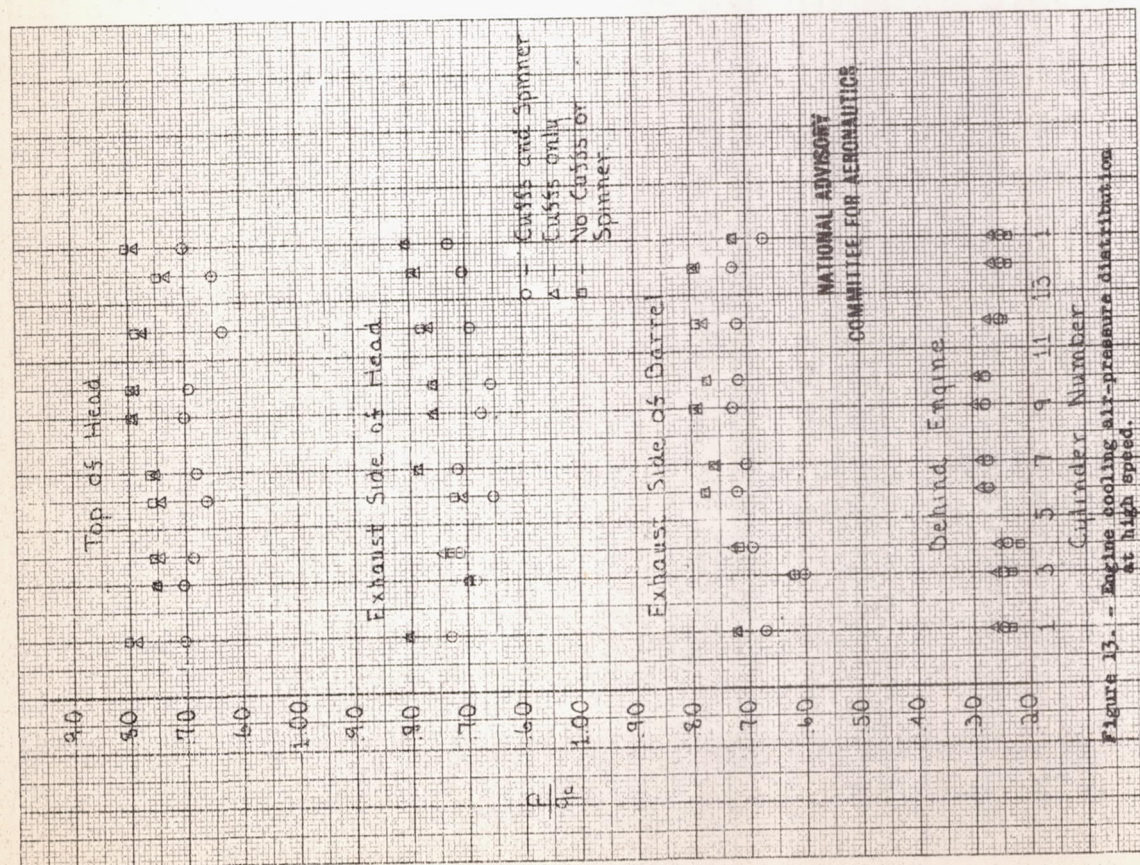


Figure 13. - Engine cooling air-pressure distribution at high speed.

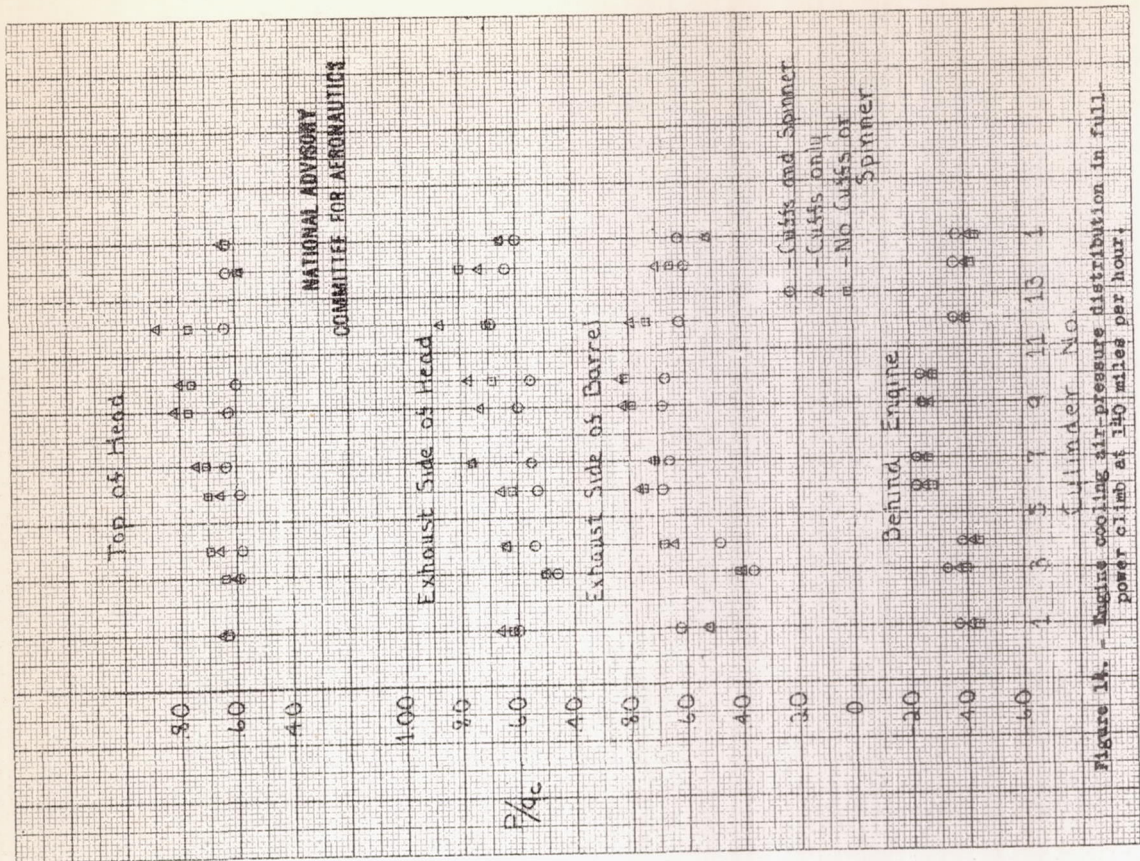
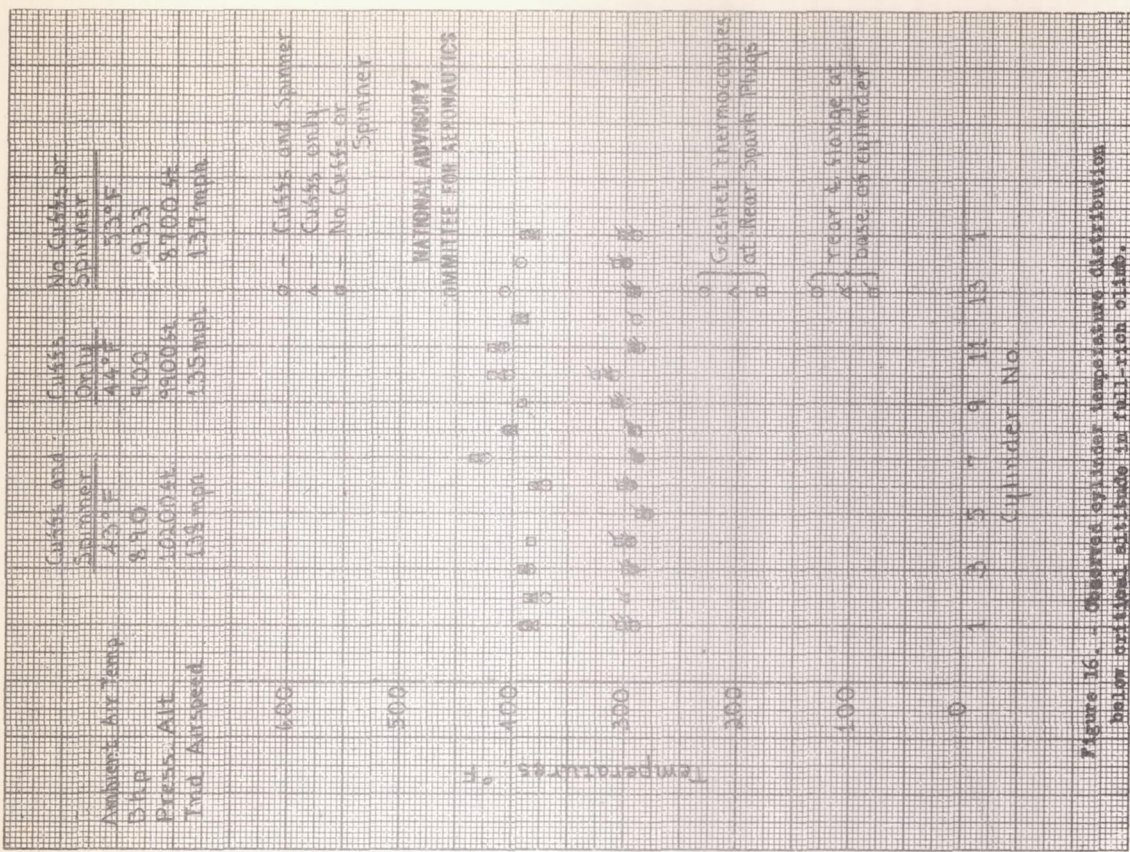
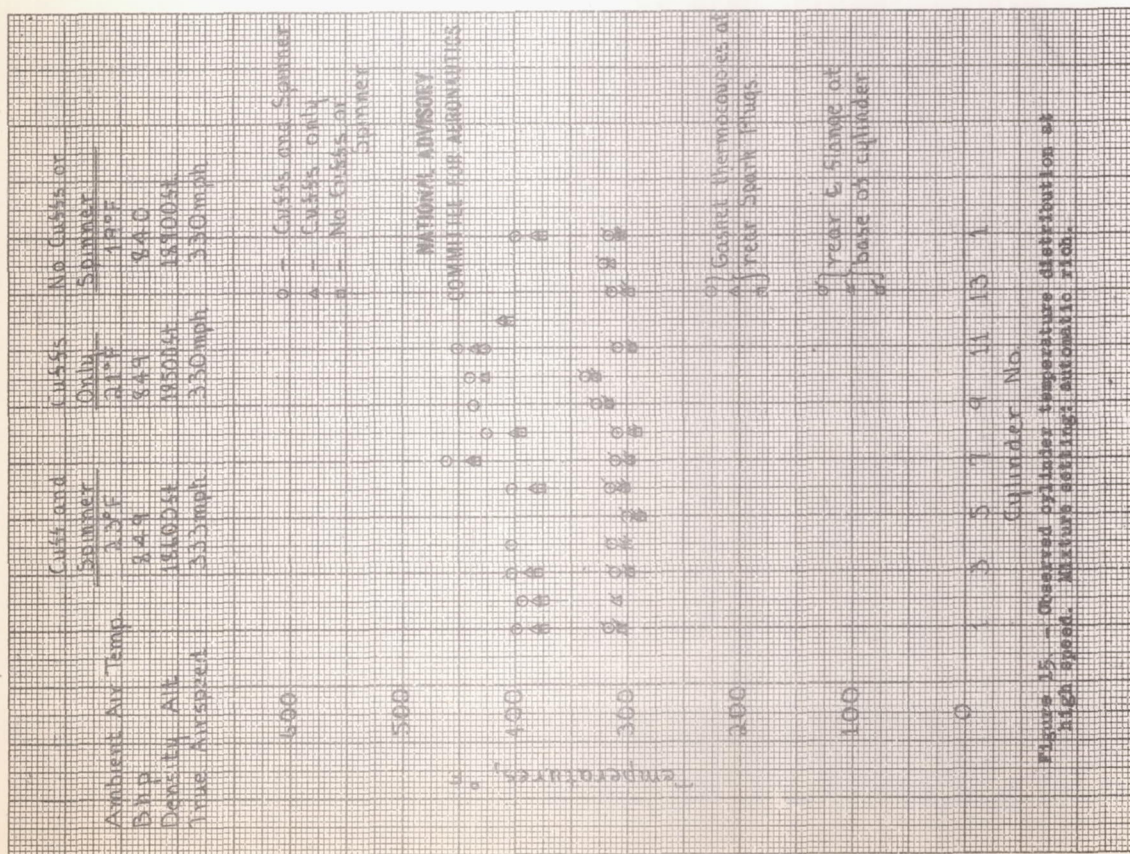


Figure 14. - Engine cooling air-pressure distribution in full-power climb at 140 miles per hour.



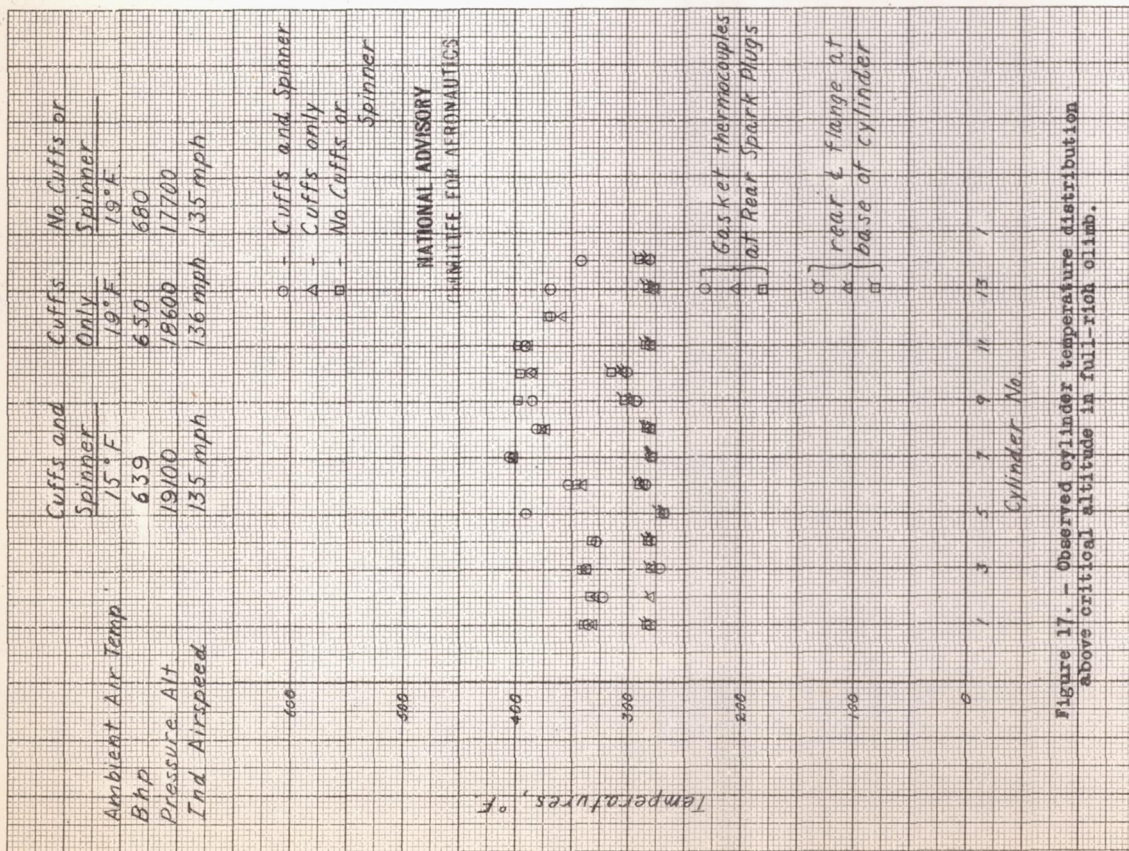


Figure 17. - Observed cylinder temperature distribution above critical altitude in full-rich climb.

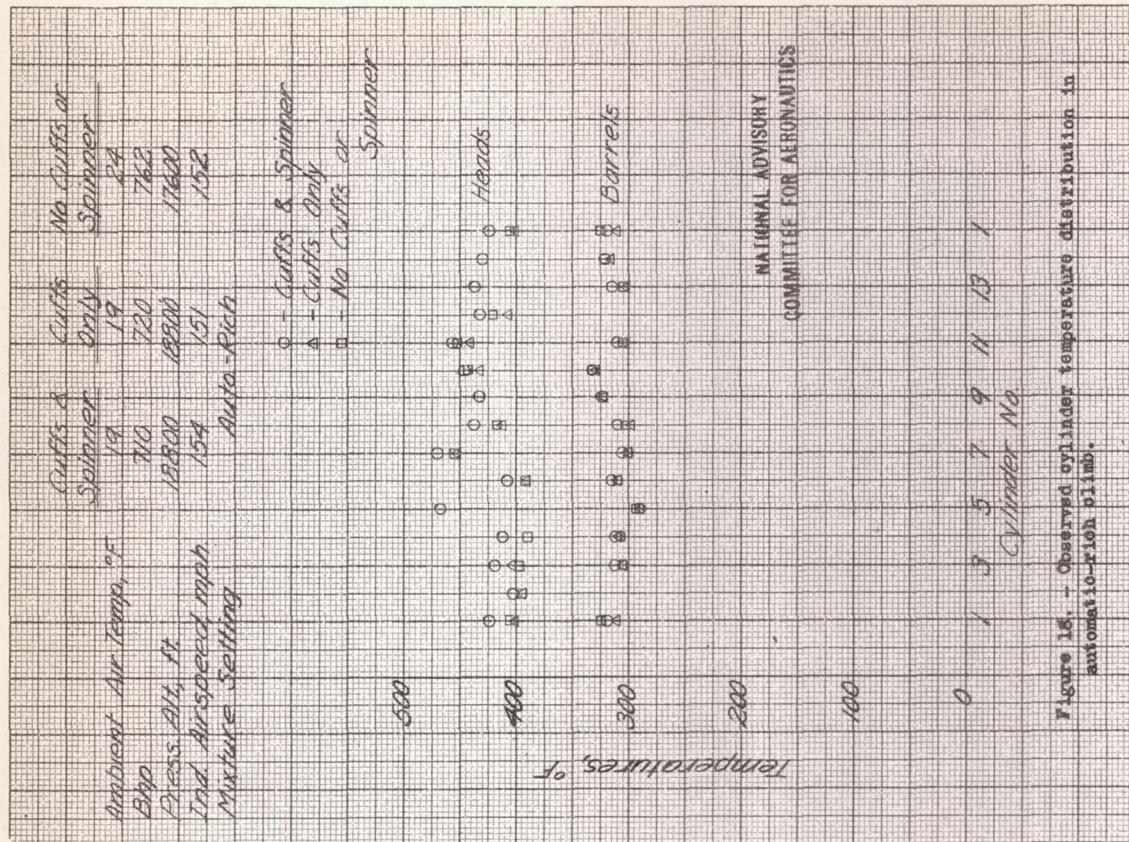


Figure 18. - Observed cylinder temperature distribution in auto-ricb climb.

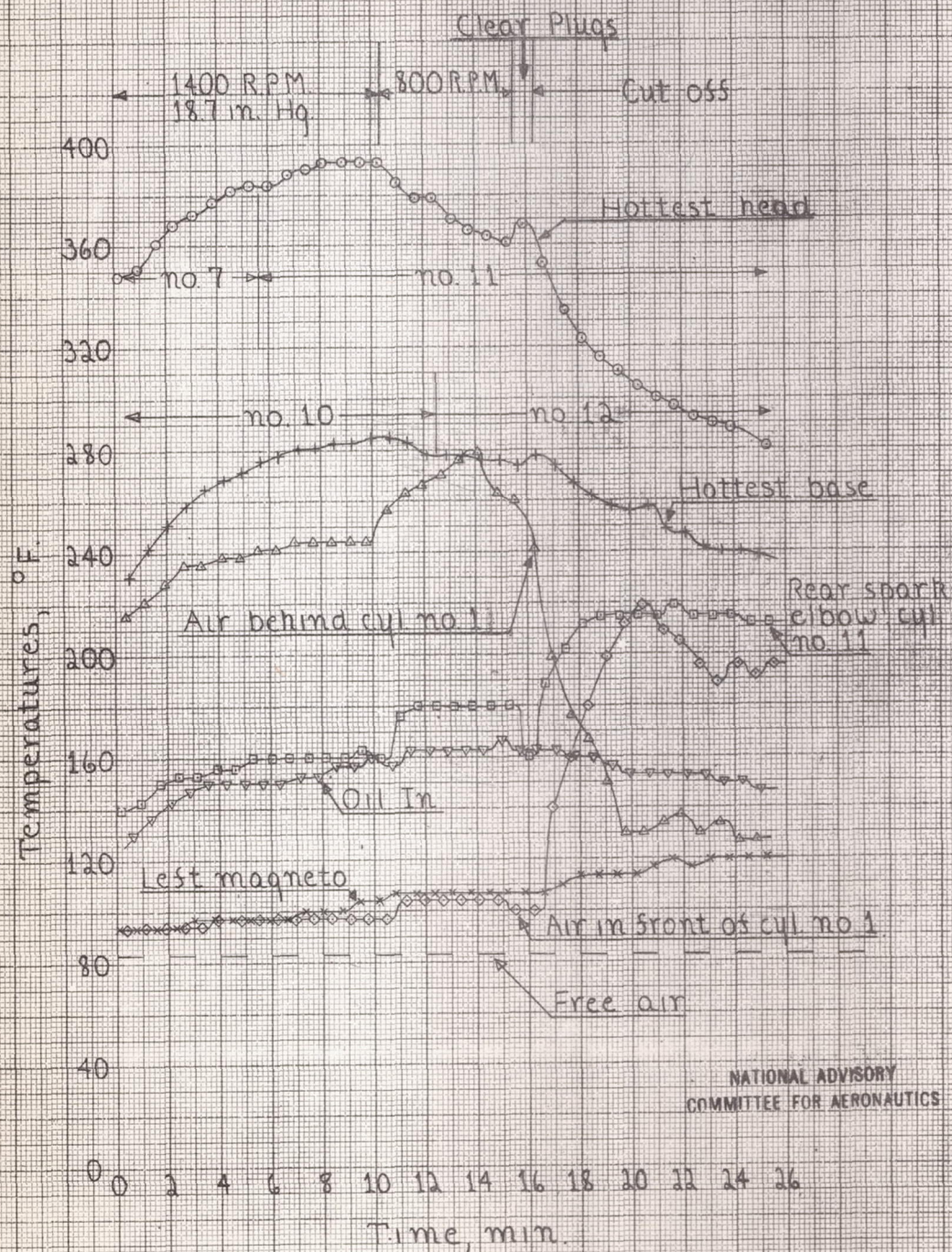


Fig. 19 - Temperatures in Ground Run with Spinner and Cussis

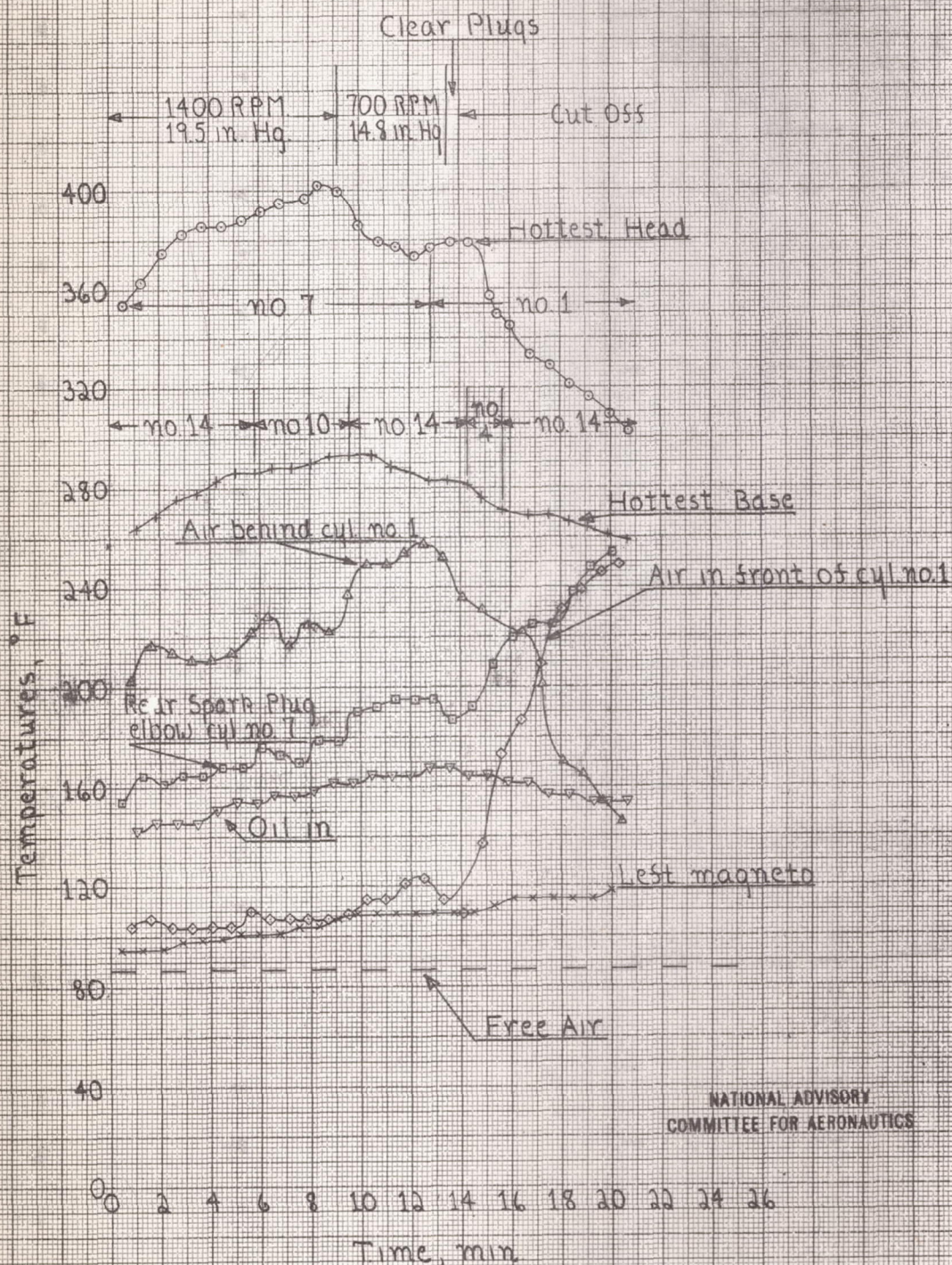


Fig. 20 - Temperatures in Ground Run with cuffs only

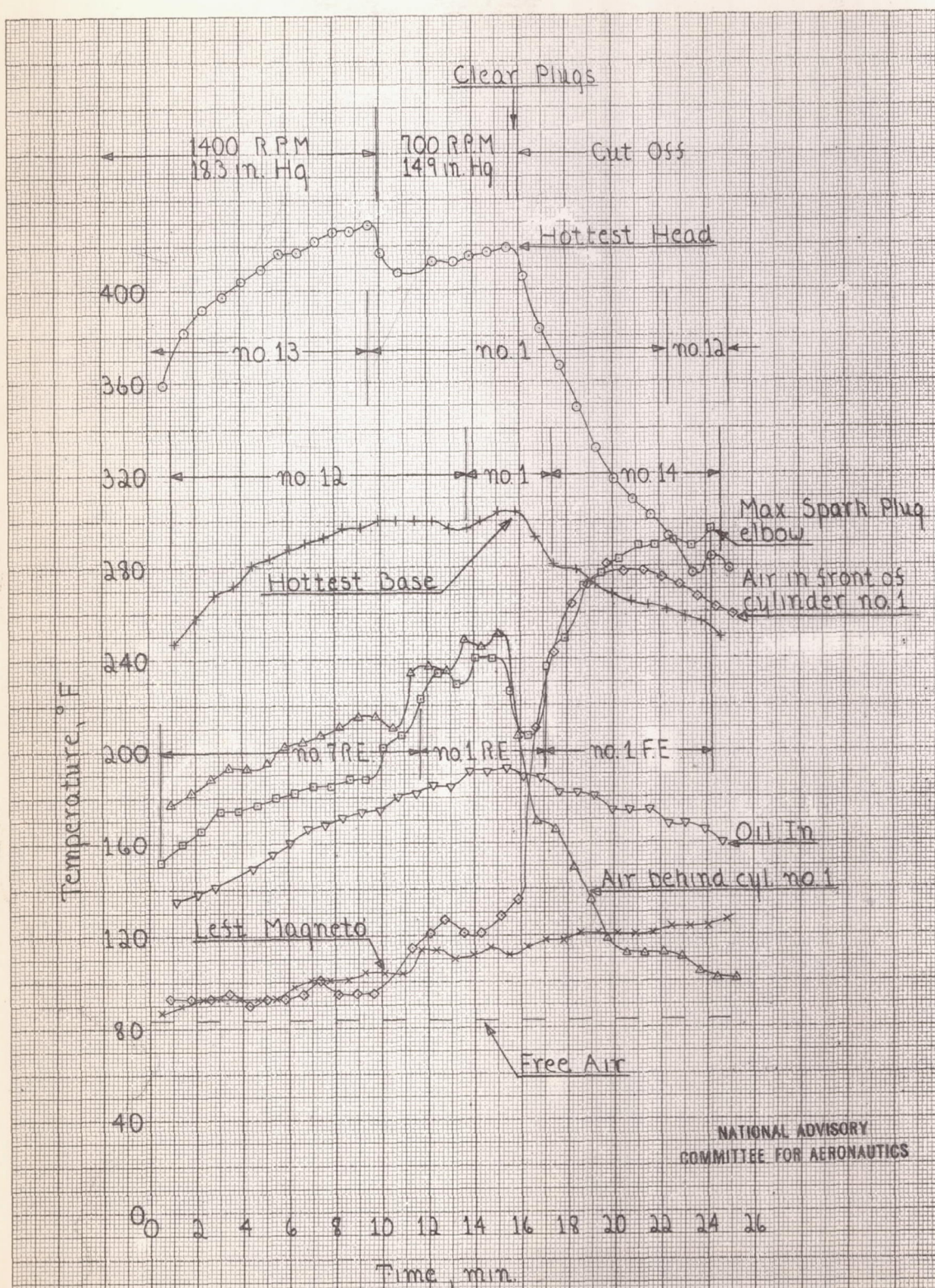


Fig 21 - Temperatures in Ground Run with no cusses
or spinner